

# The Engineering of Truly Passive Mine Water Treatment Systems using Recycled Concrete Aggregate

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## The opportunity – Gold King Mine (August 15, 2015)



*Gold King Mine portal, post-blowout*



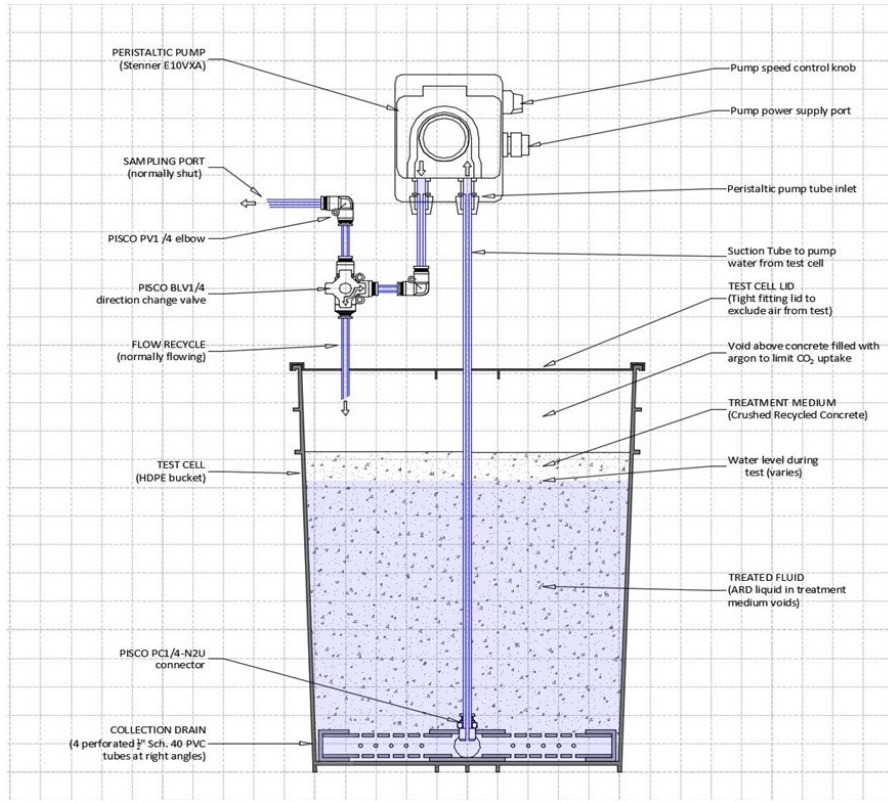
*Animas River downstream of Gold King Mine, post-blowout*

# The need, the solution, the difficulty, and the plan

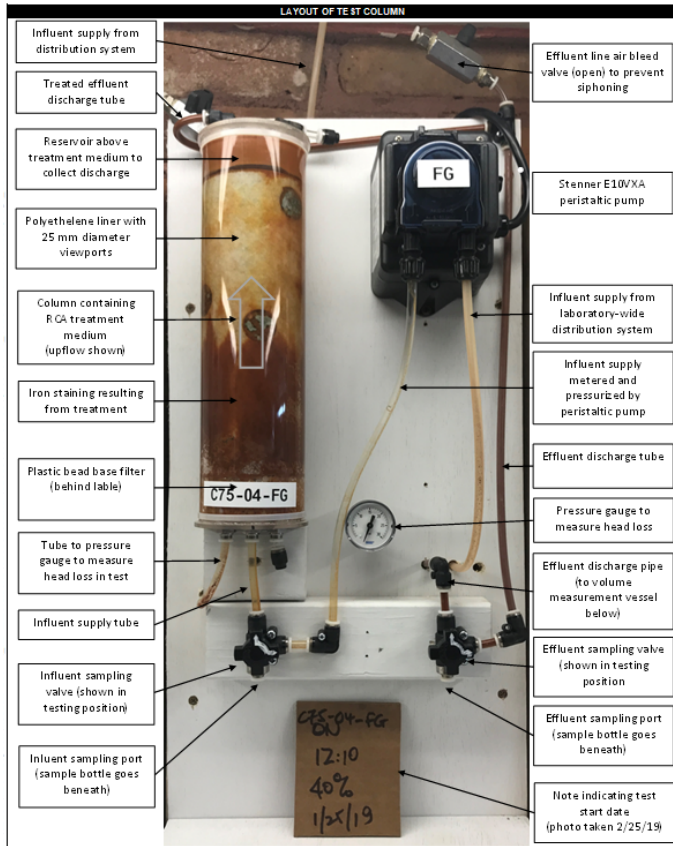


- The Need – Truly passive AMD treatment
  - A treatment method for Acid and Metalliferous Drainage (AMD) that is passive, simple, long-term, cheap, and sustainable
- The Solution - Recycled Concrete Aggregate (RCA)
  - Passive: timed release of the alkalinity in old concrete
  - Simple: pass AMD through RCA
  - Long-term: slow leach rate gives long life
  - Cheap: low cost and local short haul
  - Sustainable: recycled material with no waste
- The Difficulty - Feasibility
  - Nobody has made it work long-term
- The Plan – Learn how to make it work
  - Run actual AMD through actual RCA
  - Vary treatment rate and method till it works long-term

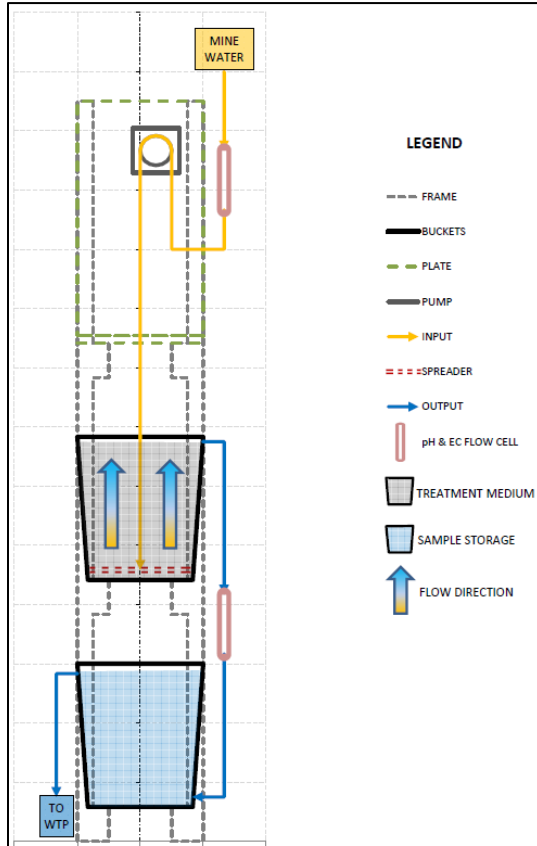
# Method #1 – Batch Testing

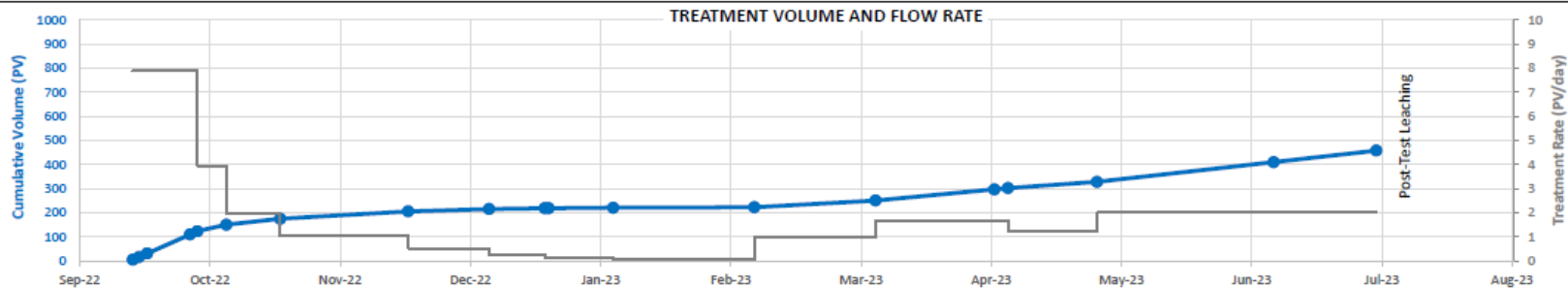


# Method #2 – Column Testing



## Method #3 – Field Testing



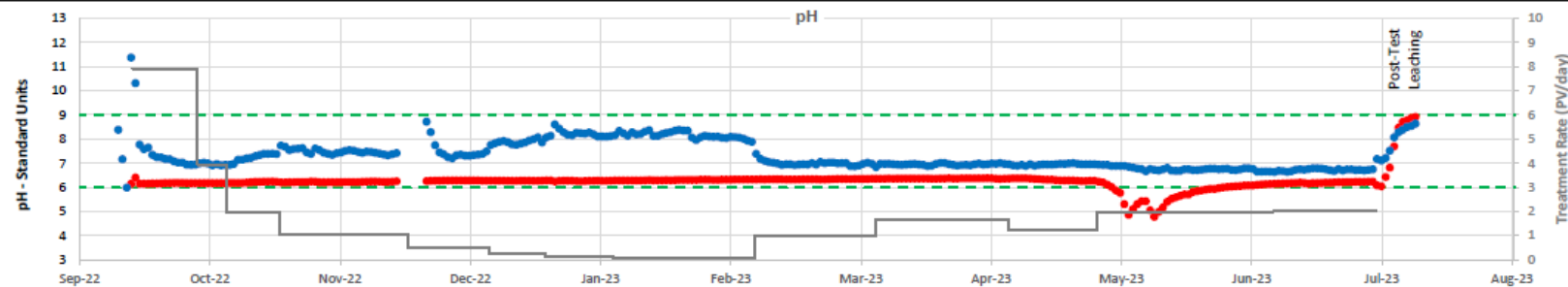


#### VOLUME TREATED

- Volume Treated (PV)  
(1 PV = 81 gallons/ton)
- Treatment Rate (PV/day)  
(1 PV/day = 0.056 gpm/ton)

**Notes:**

- Date ticks at start of month
- Sampling at end of flow period
- Retention (day) = 1/ Treatment Rate
- Linear vertical scale

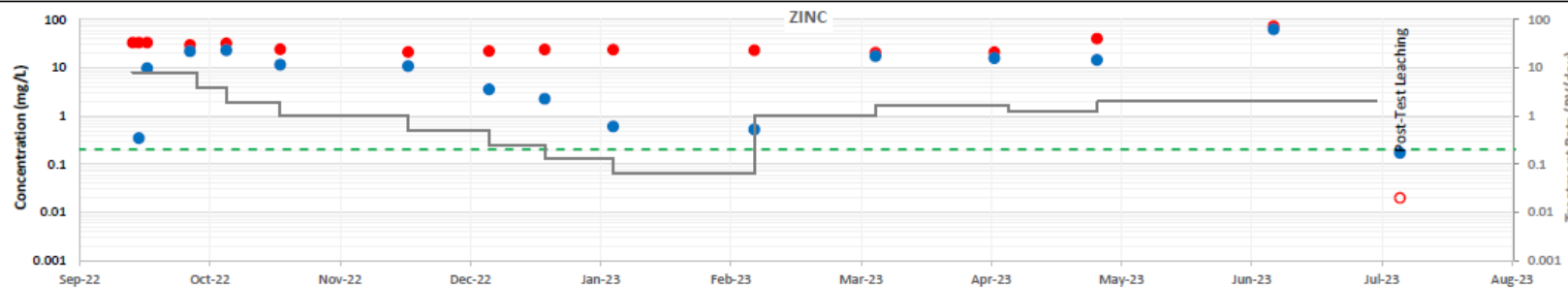


#### FLUID pH

- Eagle Mine - pH
- C18-CA Effluent - pH
- Passive Limit - pH
- Treatment Rate (PV/day)

**Notes:**

- Date ticks at start of month
- Daily average of hourly pH plotted
- Gap 11/22 due to frozen input line
- 07/23 period is freshwater leach



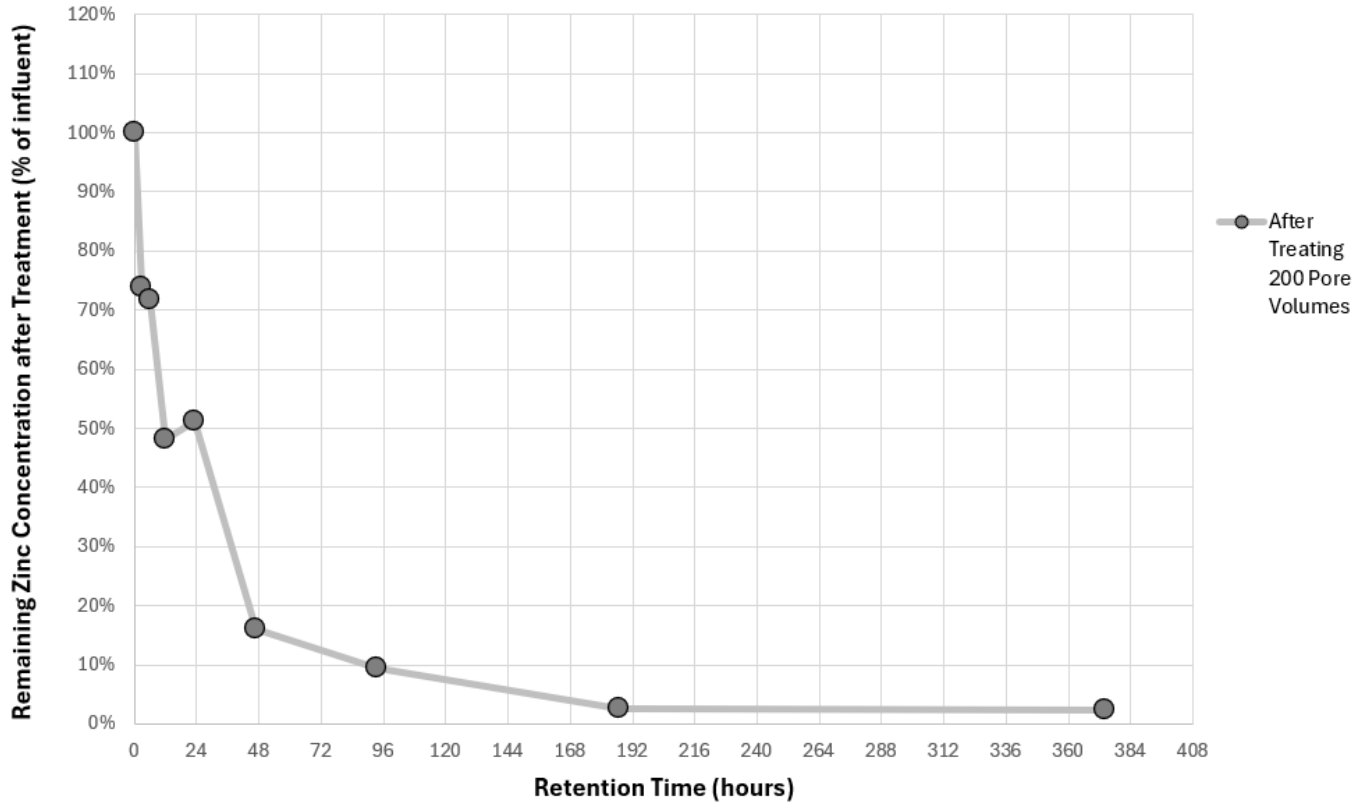
#### ZINC

- Eagle Mine - Zn (mg/L)
- C18-CA Effluent - Zn (mg/L)
- Passive Limit - Zn (mg/L)
- Treatment Rate (PV/day)

**Notes:**

- Open circles indicate non-detects at MDL
- Date ticks at start of month
- Logarithmic vertical scale
- Samples taken at end of flow period

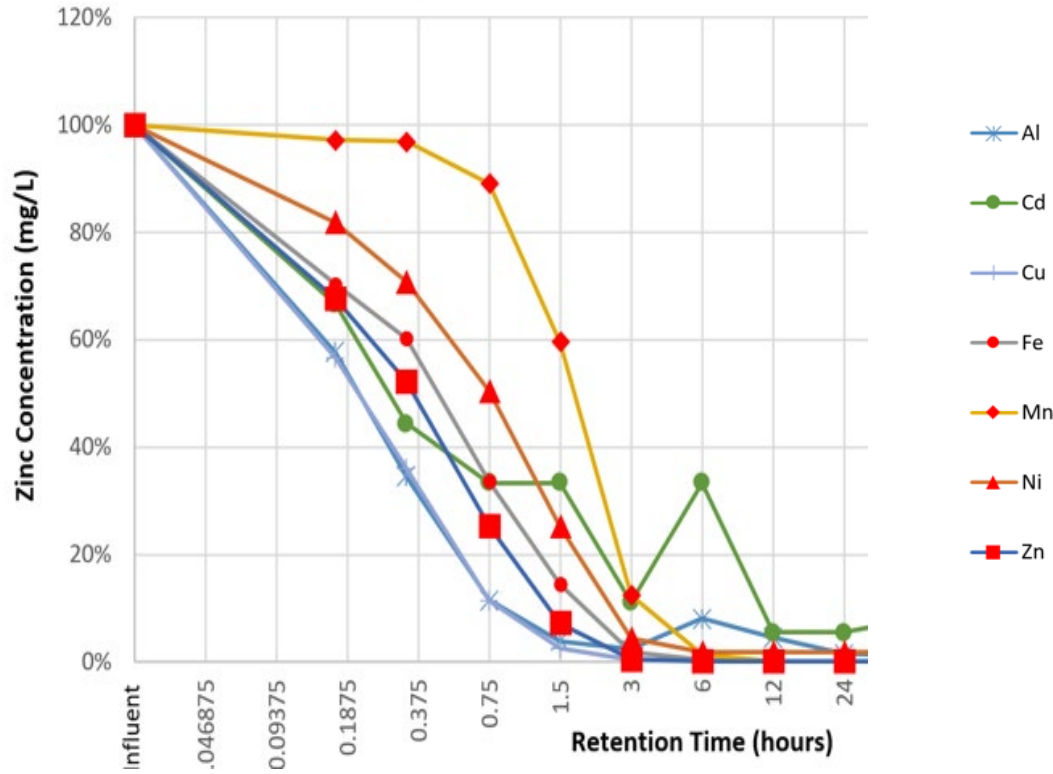
### ZINC REMOVAL AT 200 PV





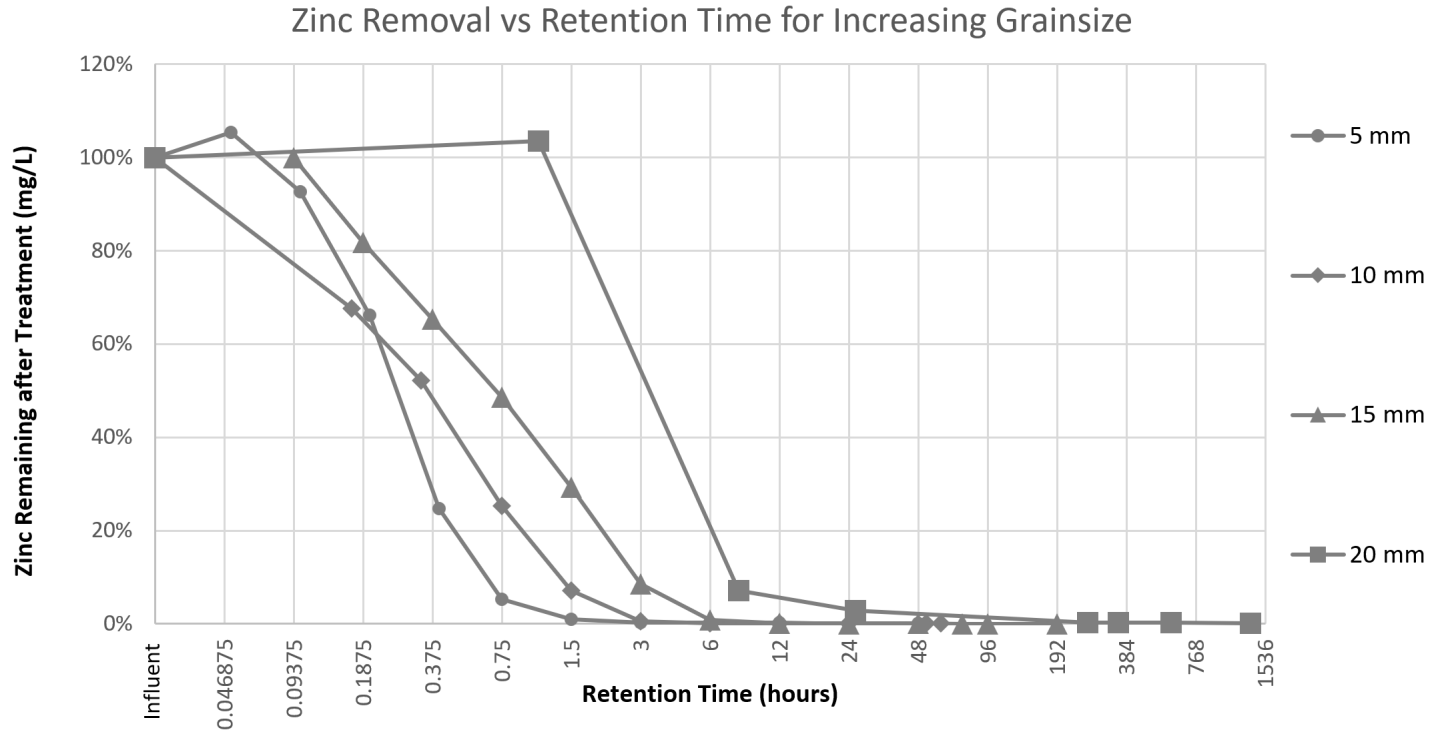
# Observation #1

# RCA successfully removes MOCs from AMD.

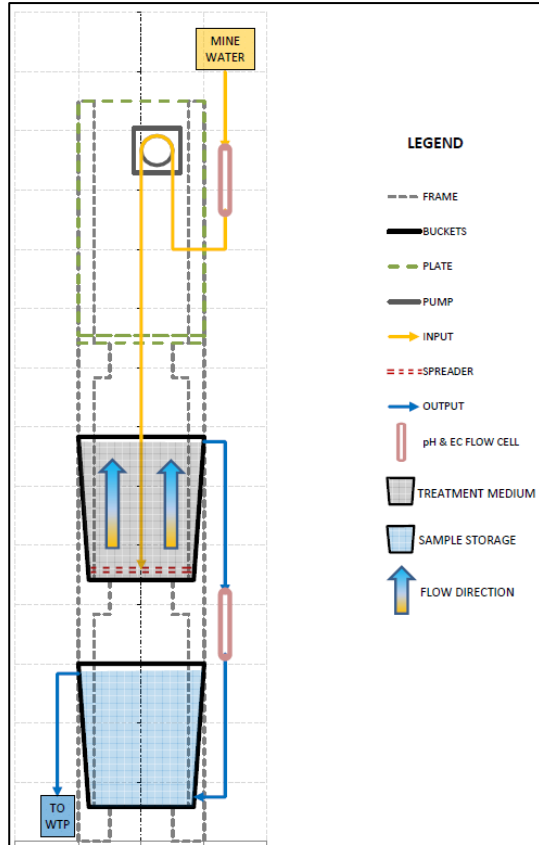


## Observation #2

## AMD treatment requires small particles of RCA



## Observation #3



## AMD treatment best with upflow through the RCA



## Observation #4

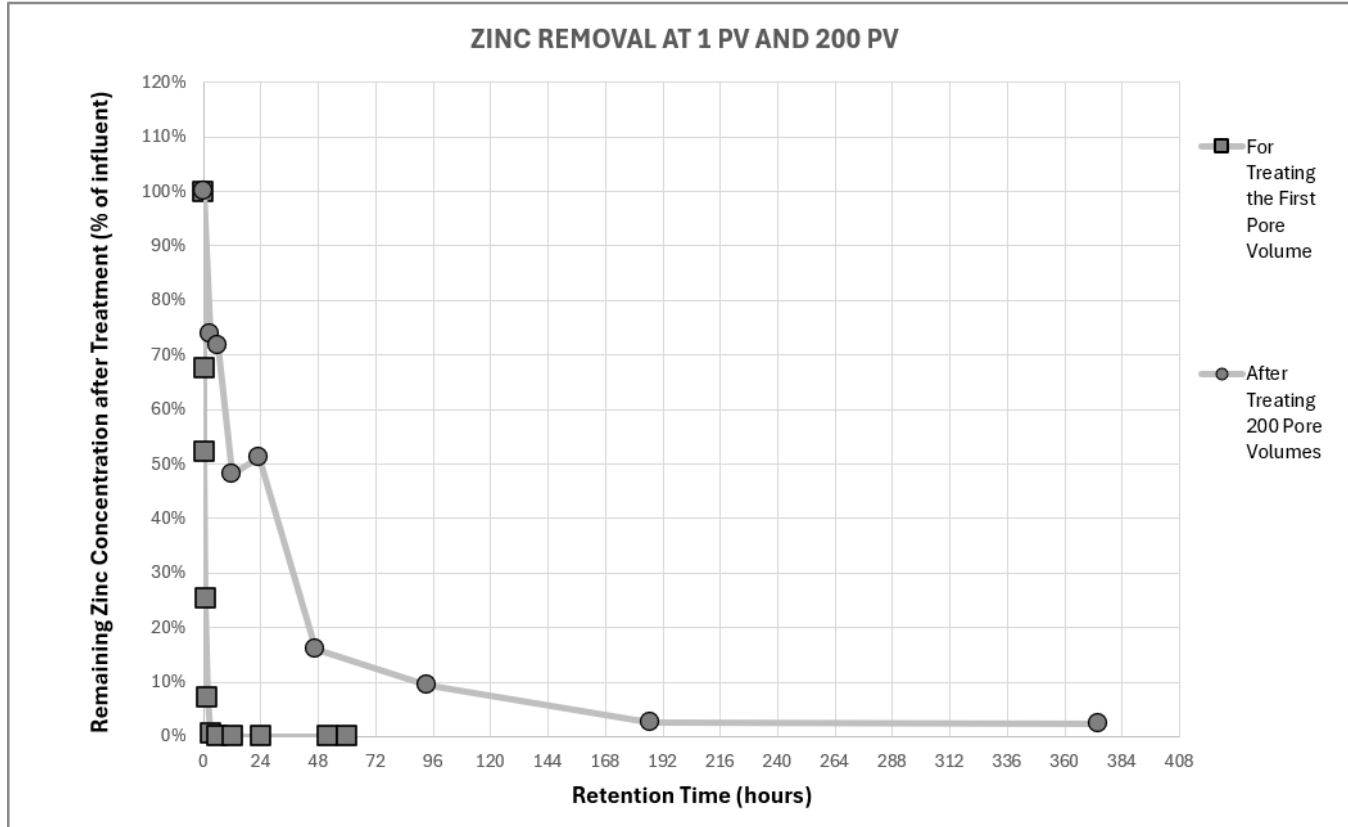


RCA treatment of AMD does not clog the RCA medium.

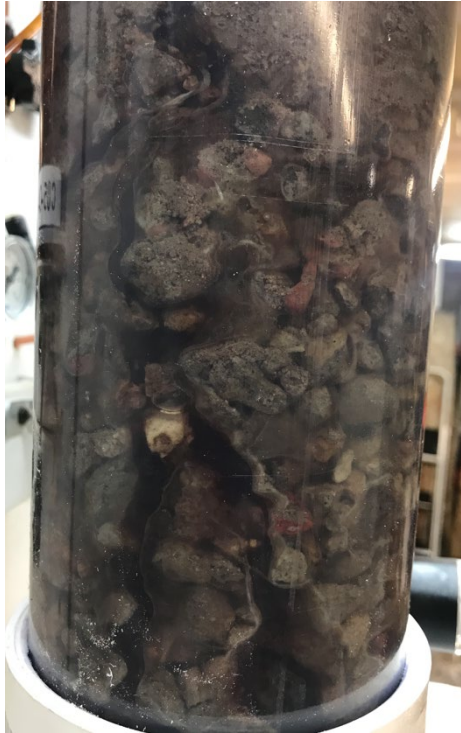


# Observation #5

# AMD treatment does not blind the RCA



## Observation #6



## RCA treatment does not create deleterious short-circuits



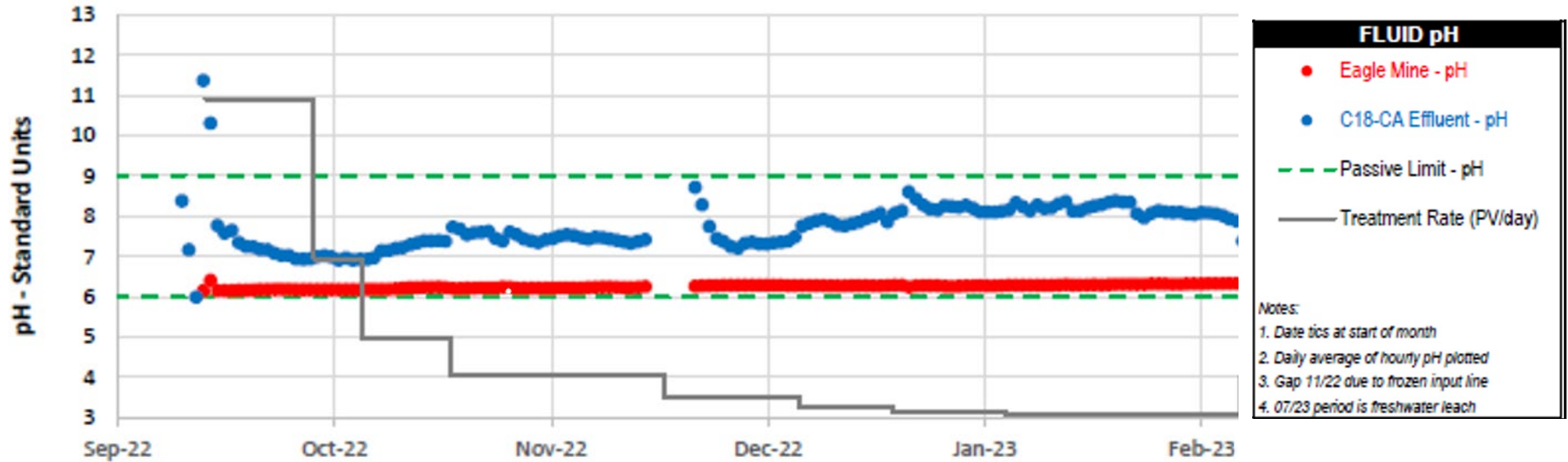
## Observation #7

## RCA treatment of AMD retains treatment products



# Observation #8

# RCA treatment of AMD produces alkaline discharge





## Observation #9

## RCA treatment of AMD permanently sequesters MOCs

<b>ELEMENT</b>	<b>PRE-TEST</b>	<b>POST-TEST</b>
	mg/kg	mg/kg
Al	49,600	60,300
As	<1,020	<202
Cd	<41	<40
Ca	71,100	42,100
Cu	<51	<51
Fe	17,800	17,700
Pb	384	<152
Mg	2,690	6,620
Mn	393	654
K	32,200	29,500
Na	15,300	18,200
S	2,530	2,060
Zn	<102	1,580

## Observation #10

RCA does not add MOCs to the treated fluid.

ANALYTE		Influent	Effluent
pH		6.2	8.1
Al	mg/L	0.09	<0.05
As	mg/L	0.298	<0.04
Cd	mg/L	0.0469	<0.008
Cu	mg/L	0.164	<0.01
Fe	mg/L	47.5	1.58
Pb	mg/L	<0.03	<0.03
Mn	mg/L	15.5	3.78
S	mg/L	566	517
Zn	mg/L	23.8	0.608

1. Determine AMD flow rate ( $Q$ ) requiring treatment; sample and analyze.
2. Determine RCA to be used for passive treatment; sample and analyze.
3. Perform batch or (better) field tests to determine:
  - a. Retention time ( $t$ ) for your RCA to treat your AMD to remove MOCs.
  - b. Porosity ( $n$ ) of your RCA from volume of AMD to flood the RCA.
  - c. Dry density ( $\rho$ ) of your RCA by dividing mass by volume of test solids.
4. Calculate the amount of RCA that is required for your passive treatment system using the data that you have just obtained:

$$\text{Total volume of RCA (V)} = \frac{\text{Treatment flow rate (Q)} \times \text{Retention time (t)}}{\text{Porosity of RCA (n)}}$$

- Based on testing as described above, a treatment system might the following characteristics:
  - Treatment Flow Rate (Q)     $\sim 1,000 \text{ m}^3/\text{day}$  ( $\sim 200 \text{ USgpm}$ )
  - Critical Retention Time (t)     $\sim 4 \text{ days}$
  - Porosity of RCA (n)     $\sim 45\%$
- The critical volume of RCA required to treat this AMD is computed using the above equation:
  - *Critical volume of RCA*  $\approx \frac{1000 \text{ (m}^3/\text{day)} \times 4 \text{ (days)}}{45 \text{ (\%)}} \approx 9,000 \text{ (m}^3)$

# Conclusion

Long-term truly passive treatment of acid and metalliferous drainage (AMD) by treatment systems using recycled concrete aggregate (RCA) is feasible, provided the following guidelines are adopted:

- 1. Small RCA particle size (2 - 20 mm).*
- 2. Large RCA mass (thousands of tonnes).*
- 3. Long contact between the AMD and the RCA (1 to 15 days).*
- 4. Minimal contact of AMD with the atmosphere (upflow).*
- 5. Simple treatment system hydraulics (no pipes).*

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