West Virginia Mine Drainage Task Force Symposium Workshop:

# PHREEQ-N-AMDTreat Model to Evaluate Water-Quality Effects from Passive and Active Treatment of Mine Drainage

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Morgantown, WV, October 5, 2022





## "PHREEQ-N-AMDTREAT"

### http://amd.osmre.gov/

SITEMAP



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#### AMDTREAT 5.0.2 PLUS NOW AVAILABLE!

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TIPS HOME

AMDTreat 5.0.2 Plus corrects minor convergence issues identified during case study tests performed by the developers.

Enhancements to Version 5 of AMDTreat include incorporation of the geochemical modeling capabilities of the U.S. Geological Survey's (USGS) PHREEQ computer program to model titrations and enhancement to the oxidant tool.

For additional information, please contact Brent Means or Omar Beckford.

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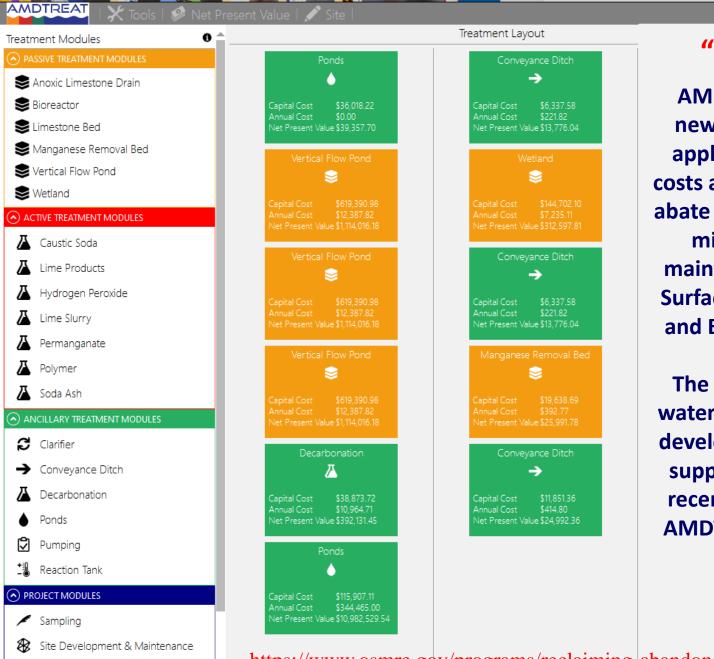
#### WHAT IS AMDTREAT?

AMDTreat (Pronounced: am'-D-treat or A-M-D-treat.), a member of OSMRE's Technical Innovation and Professional Services (TIPS) suite of software, is a computer application for estimating abatement costs for pollutional mine drainage, commonly referred to as Acid Mine Drainage or AMD. (Also Acid Rock Drainage or ARD.) The current version of AMDTreat is v5.0.2 Plus. AMDTreat can assist a user in estimating costs to abate water pollution using a variety of passive and chemical treatment types; including, vertical flow ponds, anoxic limestone drains, anaerobic wetlands, aerobic wetlands, bio reactors, manganese removal beds, limestone beds, oxic limestone channels, caustic soda, hydrated lime, pebble quicklime, ammonia, oxidation chemicals, and soda ash treatment systems. The acid mine drainage abatement cost model provides over 400 user modifiable variables in modeling costs for treatment facility construction, excavation, revegetation, piping, road construction, land acquisition, system maintenance, labor, water sampling, design, surveying, pumping, sludge removal, chemical consumption, clearing and grubbing, mechanical aeration, and ditching. AMDTreat also contains several financial and scientific tools to help select and plan treatment systems. These tools include a long-term financial forecasting module, an acidity calculator, a sulfate reduction calculator, a Langelier saturation index calculator, a mass balance calculator, a passive treatment alkalinity calculator, an abiotic homogeneous Fe2+ oxidation calculator, a biotic homogeneous Fe2+ oxidation calculator, an oxidation tool, and a metric conversion tool.

AMDTreat is a computer application for estimating abatement costs for AMD (acidic or alkaline mine drainage).

#### AMDTreat is maintained by OSMRE.

The *obsolete* version of AMDTreat 5.0+ has been recoded from FoxPro to C++ to facilitate its use on computer systems running Windows 10. *One of three* PHREEQC geochemical models described below has been incorporated to run with the recoded AMDTreat 6.0 program.



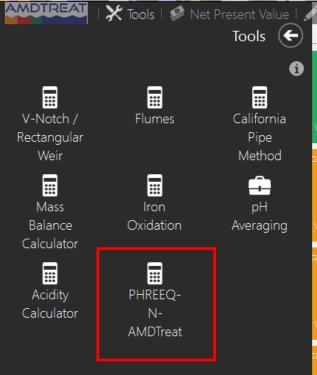
Labor

### "AMDTreat 6.0"

AMDTreat 6.0 (2022) is a newly updated computer application for estimating costs and sizing of facilities to abate AMD (acidic or alkaline mine drainage) that is maintained by the Office of Surface Mining Reclamation and Enforcement (OSMRE).

The PHREEQ-N-AMDTreat water-quality modeling tool, developed by the USGS with support from OSMRE, was recently incorporated with AMDTreat 6.0 (beta version shown here).

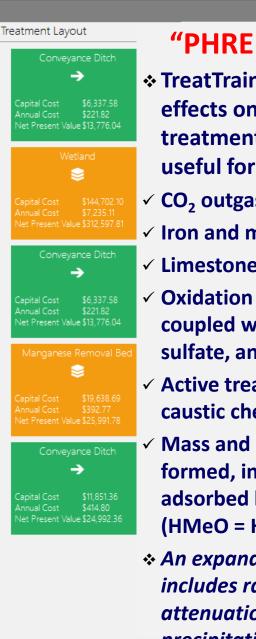
https://www.osmre.gov/programs/reclaiming-abandoned-mine-lands/amdtreat



Cravotta, C.A. III, 2020. Interactive PHREEQ-N-AMDTreat water-quality modeling tools to evaluate performance and design of treatment systems for acid mine drainage (software download): U.S. Geological Survey Software Release. https://doi.org/10.5066/P9QEE3D5

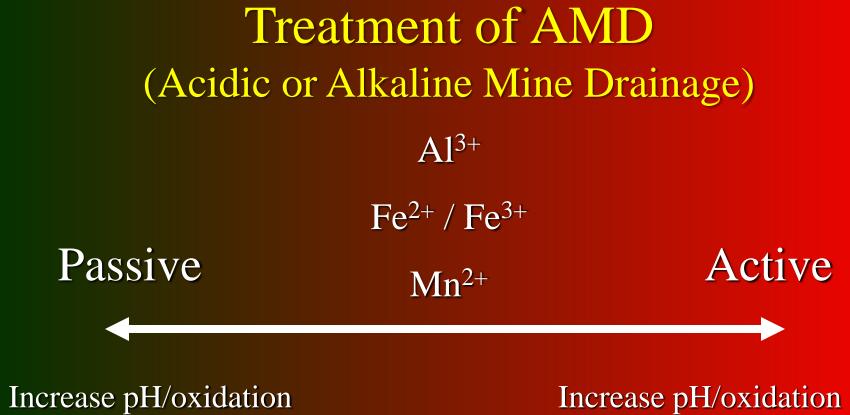
Cravotta, C.A. III, 2021. Interactive PHREEQ-N-AMDTreat water-quality modeling tools to evaluate performance and design of treatment systems for acid mine drainage: Applied Geochemistry, 126, 10845. https://doi.org/10.1016/j.apgeochem.2020.10 4845





### "PHREEQ-N-AMDTreat"

- TreatTrainMix2 model simulates effects on water quality by treatment system components; useful for costs/benefits analysis.
- $\checkmark$  CO<sub>2</sub> outgassing and O<sub>2</sub> ingassing;
- Iron and manganese oxidation;
- Limestone dissolution;
- Oxidation of organic carbon coupled with reduction of Fe<sup>III</sup>, sulfate, and nitrate.
- Active treatment with H<sub>2</sub>O<sub>2</sub> and/or caustic chemicals.
- Mass and composition of solids formed, including Fe, Mn, and Al adsorbed by hydrous metal oxides (HMeO = HFO + HMO + HAO).
- An expanded stand-alone model includes rare-earth elements attenuation by adsorption and precipitation.



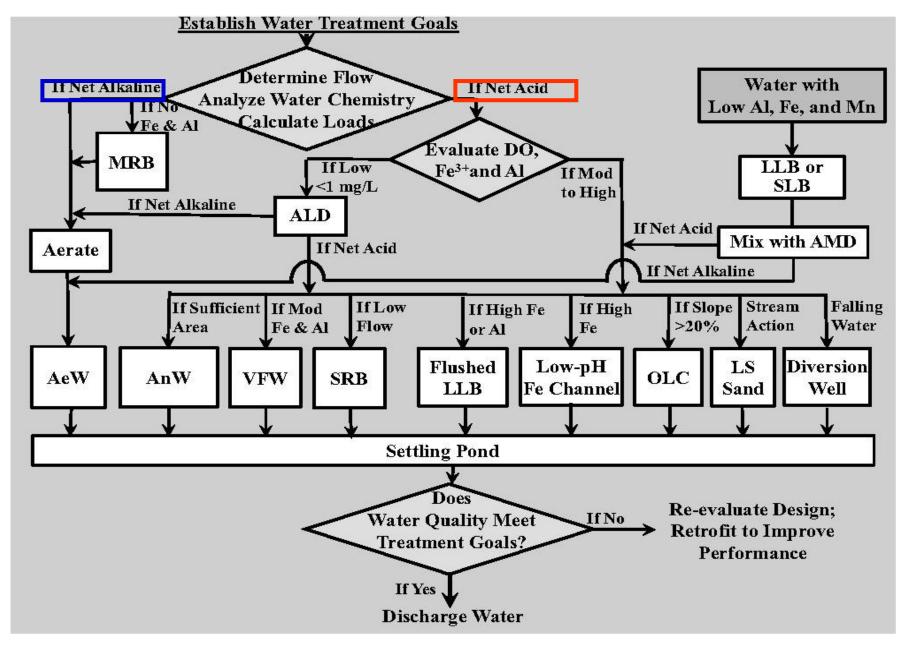
Increase pH/oxidation with aeration, natural substrates & microbes

**Reactions slow** 

Large area footprint

Low maintenance

Increase pH/oxidation with aeration &/or industrial chemicals Reactions fast, efficient Moderate area footprint High maintenance



Skousen, J.G., Zipper, C.E., Rose, A.W., Ziemkiewicz, P.F., Nairn, R., McDonald, L.M., and Kleinmann, R.L., 2017. Review of passive systems for acid mine drainage treatment. Mine Water Environ. 36, 133-153.

## **PHREEQ-N-AMDTreat Models**

Simulate water-quality changes during passive and active treatment.

Three complementary, user-friendly tools use same thermodynamic database and input water-quality data for a given AMD:

"CausticTitration.exe"

- ✓ "ParallelTreatment.exe"
- $\checkmark$  "TreatTrainMix2.exe" ( $\rightarrow$  incorporated with AMDTreat 6.0)

Graphical and tabular output indicates changes in pH, concentrations of metals, TDS, and SC plus the cumulative quantity of precipitated solids as a function of retention time or the amount of caustic added.

Evaluate design/performance and costs/benefits of alternatives.

### PHREEQ-N-AMDTreat: Modeled Variables

	Variable on User	_
Variable description	Interface	
Solutions A and B*		<ul> <li>Input water-quality, one or two solutions (A+B)</li> </ul>
Design flow	Design flow (gpm)*	
Mix fraction	Mix Fraction	_
Water temperature	Temp (C )	
Specific conductance at 25C	SC (uS/cm)	
Dissolved oxygen	DO (mg/L)	
рН	рН	
Acidity	Acidity (mg/L)	
Net acidity, calculated	Estimate NetAcidity	
Alkalinity	Alk (mg/L)	
Total inorganic carbon	TIC (mg/Las C)	
Total inorganic carbon, calculated	Estimate TIC	
Total iron	Fe (mg/L)	
Ferrous iron	Fe2 (mg/L)	
Ferrous iron, calculated	Estimate Fe2	
Aluminum	Al (mg/L)	
Manganese	Mn (mg/L)	
Sulfate	SO4 (mg/L)	
Chloride	Cl (mg/L)	
Calcium	Ca (mg/L)	
Magnesium	Mg (mg/L)	
Sodium	Na (mg/L)	-
Potassium	K (mg/L)	
Silicon	Sî (mg/L)	
Nitrate	NO3N (mg/L)	
Total dissolved solids	TDS (mg/L)	
Dissolved organic carbon	DOC (mg/L as C)	
Humate	Humate (mg/L as C)	
Hydrogen peroxide, calculated (after conservative mixing of A and B)	Estimate H2O2.mol/L	_
Kinetic adjustment factor (multiplied by rate constant) applied equally to all steps of ParallelTreatment	or TreatTrainMix2 tools	Adjustment factors for rate constants
Factor kCO2, multiplied by CO2 outgassing rate constant (kLaCO2)	factr.kCO2	-
Factor kO2, multiplied by CO2 outgassing rate constant to estimate O2 ingassing rate constant	factr.kO2	
Factor kFeHOM, multiplied by homogeneous Fe2 oxidation rate constant	factr.kFeHOM	
Factor kFeHET, multiplied by heterogeneous Fe2 oxidation rate constant	factr.kFeHET	
Factor kFellMnOx, multiplied by heterogeneous Fe2 oxidation rate constant	factr.kFellMnOx	
Factor kbact, multiplied by microbial rate constant (assumes Fe oxidizing bacteria MPN = 5.3e11 cells/	/L) factr.kbact	
Factor kFeNO3, multiplied by homogeneous Fe2 oxidation rate constant	factr.kFeNO3	
Factor kMnHOM, multiplied by homogeneous Mn2 oxidation rate constant	factr.kMnHOM	
Factor kMnHFO, multiplied by heterogeneous Mn2_HFO oxidation rate constant	factr.kMnHFO	
Factor kMnHMO, multiplied by heterogeneous Mn2_HMO oxidation rate constant	factr.kMnHMO	
Factor kSHFO, multiplied by Felll reduction-sulfide oxidation rate constant	factr.kSHFO	
Factor kSOC, multiplied by sedimentary organic carbon oxidation rate constant	factr.kSOC	
Factor kDOC, multiplied by dissolved organic carbon oxidation rate constant	factr.kDOC	
Factor kH2O2, peroxide Fe2 oxidation rate constant	factr.kFeH2O2	
Exponential factor for calcite dissolution rate model	EXPcc	

### PHREEQ-N-AMDTreat: Modeled Variables

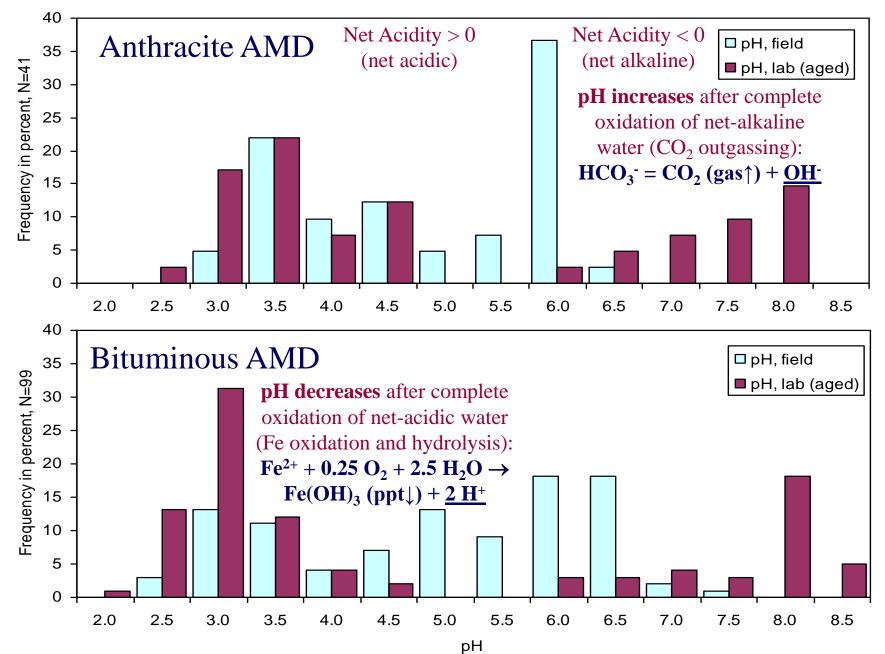
Variable description	Variable on User Interface	_
Kinetic adjustment and equilibrium variables used in CausticTitration tool		Variables applied in CausticTitration tool
Time, in seconds, for pre-aeration step	Time0	
kCO2, CO2 mass-transfer rate for pre-aeration step; see Table S6	kLaCO2.1/s	
Steady-state log PCO2, used with kCO2 in CO2 mass-transfer rate expression	Steady-state logPCO2	
Concentration of caustic soda (NaOH) solution in weight percent	NaOH wt%soln	
Equilibrium value (solid-phase precipitation limit) for all steps in CausticTitration, ParallelTreatment, or	r TreatTrainMix2 tools	Solid-phase precipitation control
Saturation index for calcite precipitation as equilibrium phase	SI_CaCO3	
Saturation index for siderite precipitation as equilibrium phase	SI_FeCO3	
Saturation index for Fe(OH)3 precipitation as equilibrium phase; see Table S2	SI_Fe(OH)3	
Saturation index for schwertmannite precipitation as equilibrium phase; see Table S2	SI_Schwertmannite	
Saturation index for Al(OH)3 precipitation as equilibrium phase; see Table S2	SI_AI(OH)3	
Saturation index for basaluminite precipitation as equilibrium phase; see Table S2	SI_Basaluminite	
Kinetic adjustment factor applied differently to each step of ParallelTreatment or TreatTrainMix2 tools	s, i = (1:11)	System variables for up to 11 treatment steps
Target pH specified for caustic addition at steps 1-5	>pH	system variables for up to 11 treatment steps
Hours total for step (1:11)	Time.hrs	
Water temperature at end of step (1:11)	Temp2.C	
Hydrogen peroxide at beginning of step (1:11)	H2O2.mol	
kCO2, CO2 mass-transfer rate at beginning of step (1:11); see Table S6	kLaCO2.1/s	
Steady-state log PCO2, used with kCO2 in CO2 mass-transfer rate expression for each step (1:11)	Lg(PCO2.atm)	
Calcite unit surface area at beginning of step (1:11); see Table S7	SAcc.cm2/mol	
Calcite mass fraction in limestone at beginning of step (1:11)	M/M0cc	
Sedimentary organic carbon mass at beginning of step (1:11)	SOC.mol	
Sorbent mass at beginning of step (1:11)	HMeO.mg	
Sorbent content as percent iron at beginning of step (1:11)	Fe%	
Sorbent content as percent manganese at beginning of step (1:11)	Mn%	
Sorbent content as percent aluminum at beginning of step (1:11)	Al%	
Description of step (1:11)	Description	

\*Input values for two different solutions, A and B, may be entered. Suffix "B" applies to variable names for solution B.

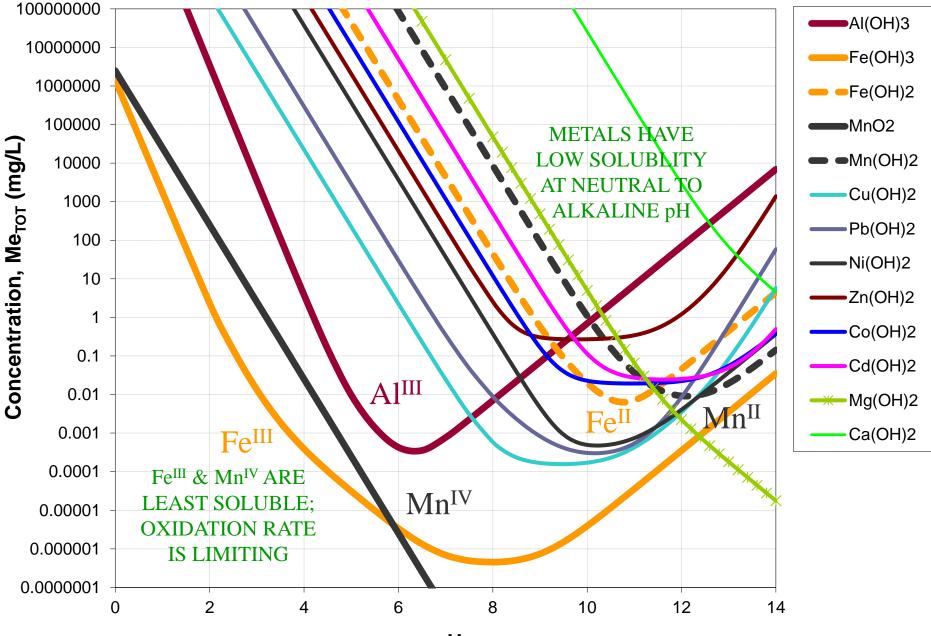
## pH, Oxidation State, and Speciation Affect Attenuation of Metals



Bimodal pH, Net Acidic, and Net Alkaline AMD

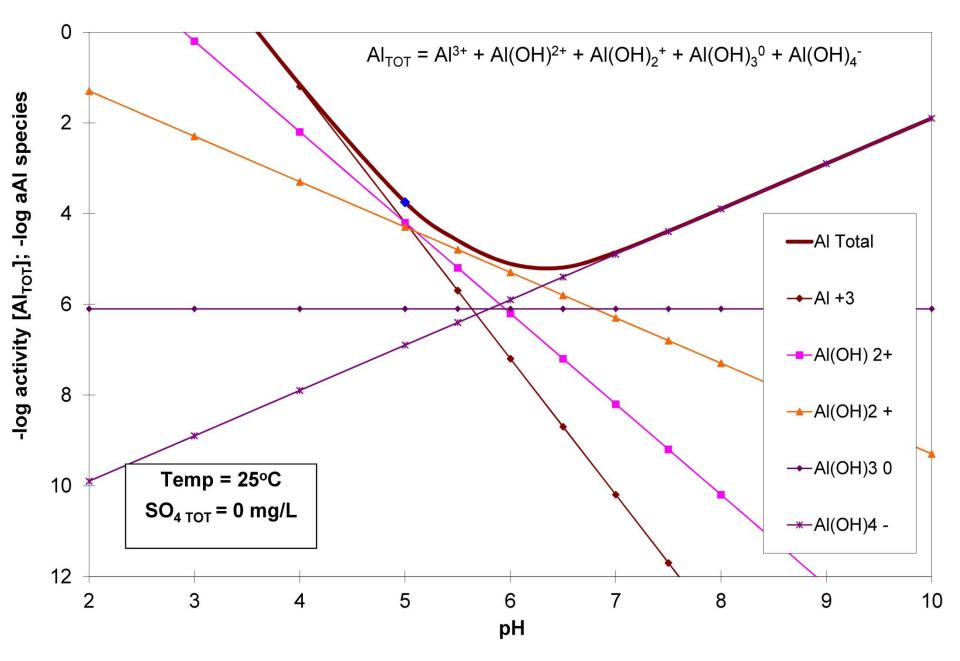


### Solubilities of Metal Hydroxides

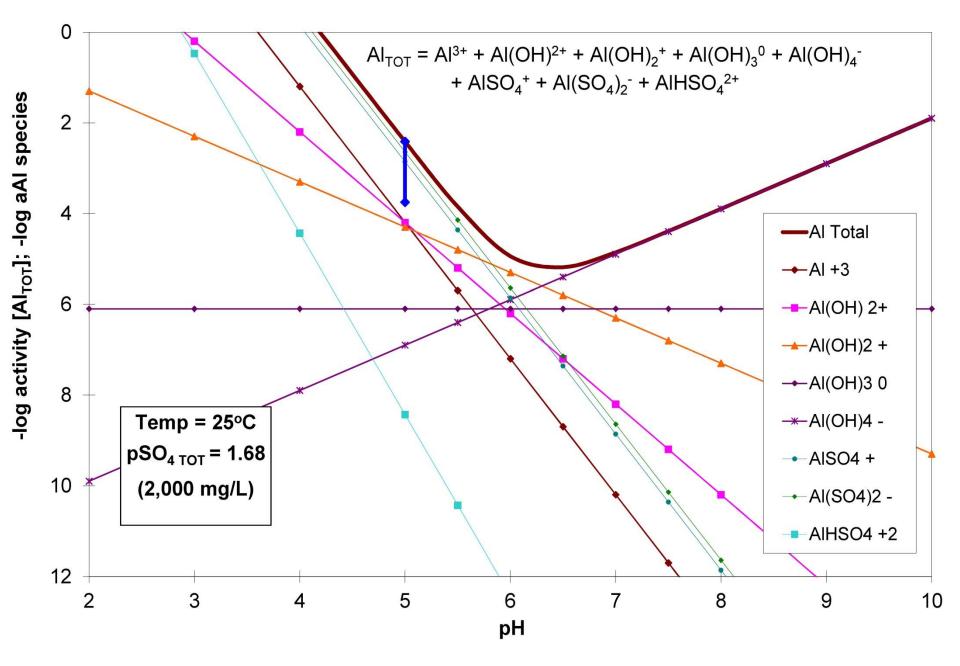


pН

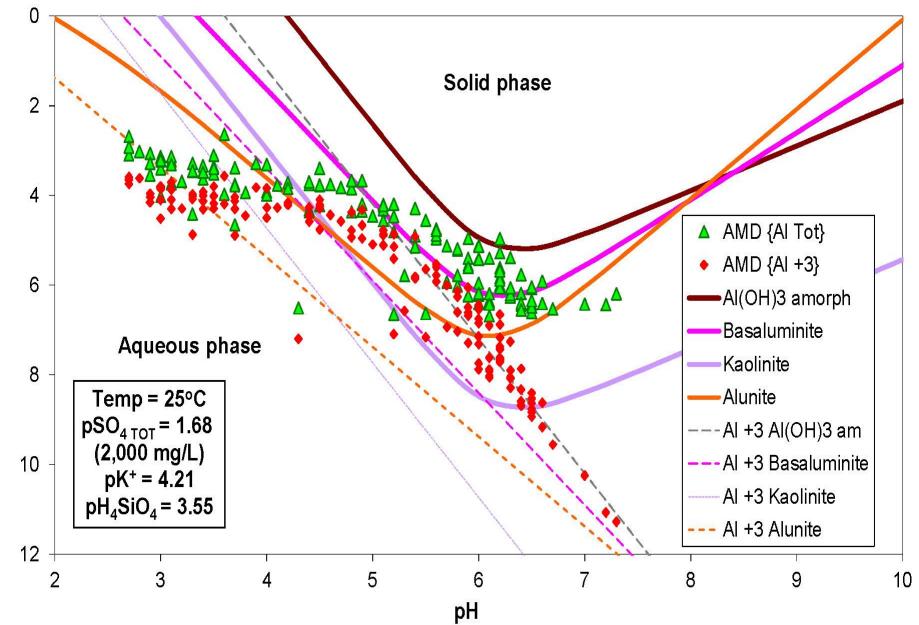
### Al Solubility



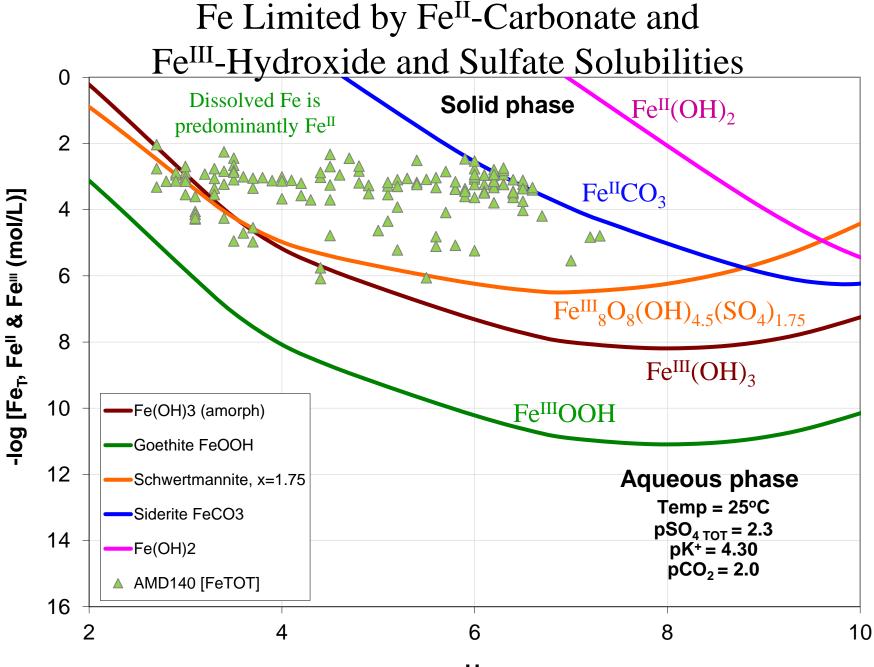
### Al Solubility Considering Aqueous Sulfate Species



### Al Solubility Considering Aqueous Sulfate Species



-log activity Al<sub>τoτ</sub> or Al<sup>+3</sup>



рΗ

Iron Oxidation Kinetics are pH Dependent (pH is affected by gas exchange, hydrolysis, neutralization; abiotic and microbial processes can be involved)

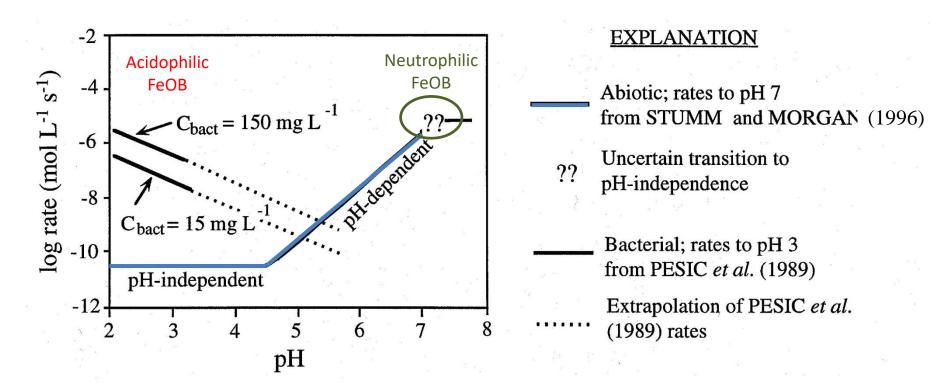


Fig. 3. Rate of Fe(II) oxidation versus pH based on abiotic and biological rate laws (Kirby et al., 1999)

\*\* C<sub>bact</sub> is concentration of iron-oxidizing bacteria (FeOB), in mg/L, as dry weight of bacteria (2.8E-13 g/cell or 2.8E-10 mg/cell).

The AMDTreat FeII oxidation kinetic model uses most probable number of iron-oxidizing bacteria per liter (MPNbact).

 $C_{bact}$  = 150 mg/L is equivalent to MPNbact = 5.3E11, where Cbact = MPNbact ·(2.8E-10).

Neutrophilic rate is adjusted for optimum conditions of pH (6.5-7.5) and low DO (1.9-2.2 mg/L) (Eggerichs et al., 2014). Additionally, catalysis by adsorption to solids (heterogeneous oxidation) depends on pH (>5).

## **PHREEQ-N-AMDTreat Examples** Gas Exchange, pH, and Metals Attenuation



### Caustic Titration with Pre-Aeration (Decarbonation) St. Michael: pre-aeration decreases CO<sub>2</sub> acidity, caustic usage, and sludge File Select folder for input/output water-quality

Select Workspace	C:\Users\cravott	a\Documents\AMDTreat_geochem_c	lata\StMichael				
One or two	Soln#A	Soln#B				Options: r	no aeration,
initial solution Design flow (gpm)	S: 5200	0	Caustic Chemical Treatment Type			•	·
Mix fraction	1	0 Only Soln#A	O Hydrated Lime, Ca(OH)2			kinetic pr	e-aeration
Temp (C)	15.4	0.01	Pebble Quick Lime, CaO			$(w/wo H_2C)$	$)_{a}$ ) and
			Caustic Soda, NaOH 2	20 v wt% soln		` <u> </u>	<u> </u>
SC (uS/cm)	1923	0	Soda Ash, Na2CO3			equilibriun	n aeration.
DO (mg/L)	0.01	0.01 DO must be > 0					
pН	5.7	0	Not Aerated     Instant	aneous equilibratio			
Acidity (mg/L)	254.2	0	Pre-Aerated Time Secs	54 Duratio	on of pre-aeration in	sec	
Estimate NetAcid	dity 223	0	kLaCO2.1/s	0.05 v CO <sub>2</sub> ou	tgassing rate constar	nt in sec <sup>-1</sup>	
Alk (mg/L)	50.8	0	factr.kCO2	1 Adjusti	ment CO <sub>2</sub> outgassing	rate (x kLaCO2)	
TIC (mg/L as C)	57.3	0	factr.kO2	2.1 Adjustr	ment O <sub>2</sub> ingassing rat	te (x kLaCO2)	
Estimate TIC	63.5	0	H2O2.mol (	0 Hydrog	gen peroxide added*		
Fe (mg/L)	148	0	Estimate H2O2.mol/L	0.001332 *multij	ply Fe2.mg by 0.0000	009 to get [H <sub>2</sub> O <sub>2</sub> ]	
Fe2 (mg/L)	148	0	0.0001143 35wt% 0.0001	082 50wt%		Allows sele	ection and
Estimate Fe2	0	0	H2O2 wt% units gal/gal (mem	no, not used)			
AI (mg/L)	0.34	0	factr.kFeH2O2	1 Adjust	ment to H <sub>2</sub> O <sub>2</sub> rate	evaluation	of key variables
Mn (mg/L)	3.6	0	O Aerated to Equilibrium Equilib	ration with specifie	ed log(Pco <sub>2</sub> , atm)	that affect	chemical usage
SO4 (mg/L)	1078	0	User Specified "Steady-State	" Conditions:		efficiency.	Ŭ
CI (mg/L)	32.8	0		-3.4 ~		chickency.	
Ca (mg/L)	242	0	Steady-state logPCO2	S	elected mineral		
Mg (mg/L)	88.7	0	Saturation Index Ig(IAP/K) to Preci	pitate Selected Solids: p	precipitation points	Cravotta, C.A	. III, 2021. Interactive
Na (mg/L)	27.8	0 Al	(OH)3 0.0 V E	Basaluminite 3.0	~	PHREEQ-N-	AMDTreat water-
K (mg/L)	9.15	Fe	e(OH)3 0.0 ~ s	Schwertmannite 1.0	~	1 V	ing tools to evaluate
Si (mg/L)	18.8	Ca	aCO3 0.3 V F	FeCO3 or MnCO3 2.5	~	1	and design of treatment
NO3N (mg/L)	0	0	Consulta Theritan O taut		onal report of output	<i></i>	cid mine drainage:
TDS (mg/L)	0		Generate Titration Output		IREEQC Output Report	* *	chemistry, 126, 10845.
				Plot Sat Index	Plot PPT Solids	1 0	g/10.1016/j.apgeochem.
DOC (mg/L as C)	0.1	· · ·	nal on-screen graphical display	s of selected outpu	It	2020.104845	
Humate (mg/L as C)	0.1	0 Caustic Titration	n.exe created by C.A. Cravotta III, U.S. G	eological Survey. Version	n 1.4.5, August 2021		

### Caustic Titration with Pre-Aeration (Decarbonation) St. Michael: pre-aeration decreases $CO_2$ acidity, caustic usage, and sludge

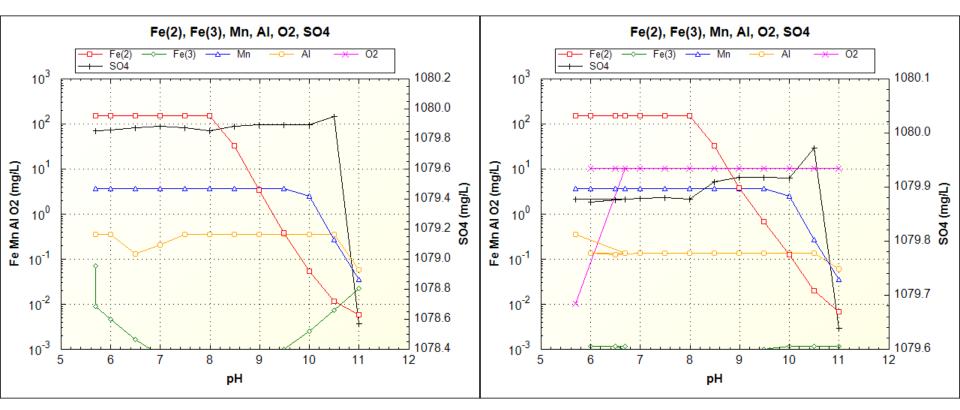
A. CausticTitration.exe: Not aerated (CaO reacted to achieve pH 8.5 is 675 mg/L as CaCO<sub>3</sub>) Caustic

A. Causti	childhon.exe.	NUL aclateu	(Cao reacted	to achieve pri	0.5 IS <b>075</b> Illg	/Las Caco <sub>3</sub> /				
pН	Caustic asCaCO3mg	Fe_mg	Fe2_mg	Al_mg	Mn_mg	TDS_mg	NetAcidity_mg	SolidsPPT_mg	CO2_mg	O2_mg
5.699391	0.000000	148.253946	148.184017	0.340583	3.606177	1,844.993285	219.160655	0.000000	184.696702	0.000000
5.698863	0.000000	148.192824	148.184017	0.340589	3.606188	1,844.843522	219.051235	0.116997	184.743198	0.000000
6.000000	36.694286	148.189513	148.184989	0.340591	3.606212	1,881.558706	182.288486	0.125192	152.974763	0.000000
6.500000	112.570987	148.188619	148.186989	0.125352	3.606260	1,956.151328	106.359043	0.753005	87.623936	0.000000
7.000000	171.880310	148.189212	148.188493	0.204352	3.606297	2,016.003903	47.027779	0.526362	37.108986	0.000000
7.500000	304.913856	148.187159	148.186724	0.340595	3.606254	1,955.324734	108.502893	194.644240	8.208932	0.000000
8.000000	420.943189	148.184464	148.184105	0.340589	3.606190	1,859.127523	204.623649	406.792768	0.939037	0.000000
8.500000	674.529768	31.972639	31.972263	0.340599	3.606297	1,671.810545	44.644131	687.418049	0.074199	0.000000
9.000000	737.552245	3.319670	3.319157	0.340602	3.606323	1,629.448665	1.378623	753.285879	0.007021	0.000000
9.500000	752.060641	0.379644	0.378671	0.340601	3.606321	1,629.762183	-7.720410	763.426508	0.000694	0.000000
10.000000	767.704290	0.055916	0.053479	0.340601	2.441687	1,639.455711	-21.535525	767.660752	0.000068	0.000000
10.500000	1,067.563230	0.018483	0.011410	0.340618	0.266277	1,695.835449	-39.623063	935.930409	0.000005	0.000000
11.000000	1,171.884112	0.027497	0.005748	0.055888	0.034796	1,729.690739	-65.761207	987.130878	0.000000	0.000000
B. Causti	cTitration.exe:	Pre-aerated,	CO <sub>2</sub> decrease	d almost 90%	(CaO reacted	to achieve pH	8.5 is <b>290</b> mg	/L as CaCO <sub>3</sub> )	_	
pН	Caustic asCaCO3mg	Fe_mg	Fe2_mg	Al_mg	Mn_mg	TDS_mg	NetAcidity_mg	SolidsPPT_mg	CO2_mg	O2_mg
5.700000	0.000000	148.253944	148.253944	0.340583	3.606177	1,796.954955	218.906769	0.000000	184.683994	0.010018
6.697709	0.000000	148.153294	148.152157	0.131429	3.606182	1,795.523678	218.803412	0.797321	17.796470	10.215814
6.000000	-28.616060	148.152569	148.151421	0.131434	3.606169	1,766.883972	247.467641	0.000009	42.257085	10.215762
6.500000	-7.568373	148.153121	148.151973	0.122499	3.606183	1,787.899450	226.379052	0.025841	24.223205	10.215800
7.000000	9.055535	148.153108	148.152391	0.131435	3.606193	1,804.585382	209.741323	0.000836	10.263163	10.215829
7.500000	18.349692	148.152996	148.152562	0.131435	3.606197	1,813.885563	200.442332	0.001376	3.580427	10.215841
8.000000	35.672893	148.152651	148.152292	0.131435	3.606191	1,810.601897	203.719540	20.603783	0.958068	10.215822
8.500000	289.472888	32.288226	32.287850	0.131439	3.606297	1,660.197303	45.284262	302.427612	0.075796	10.216122
9.000000	352.483745	3.743785	3.743272	0.131440	3.606322	1,626.972166	2.424687	368.515322	0.007173	10.216195
9.500000	367.272893	0.673854	0.672881	0.131440	3.606321	1,628.061164	-6.846925	378.974003	0.000709	10.216191
10.000000	383.349079	0.123433	0.122284	0.131440	2.431956	1,637.645626	-21.058240	383.628171	0.000070	10.216184
10.500000	683.966927	0.020465	0.019316	0.131446	0.264708	1,694.073381	-39.188404	552.424752	0.000005	10.216705
11.000000	786.717176	0.007691	0.006542	0.060071	0.034620	1,730.957523	-65.661659	598.666335	0.000000	10.216884

# Caustic Titration with Pre-Aeration (Decarbonation) St. Michael: pre-aeration decreases $CO_2$ acidity, caustic usage, and sludge



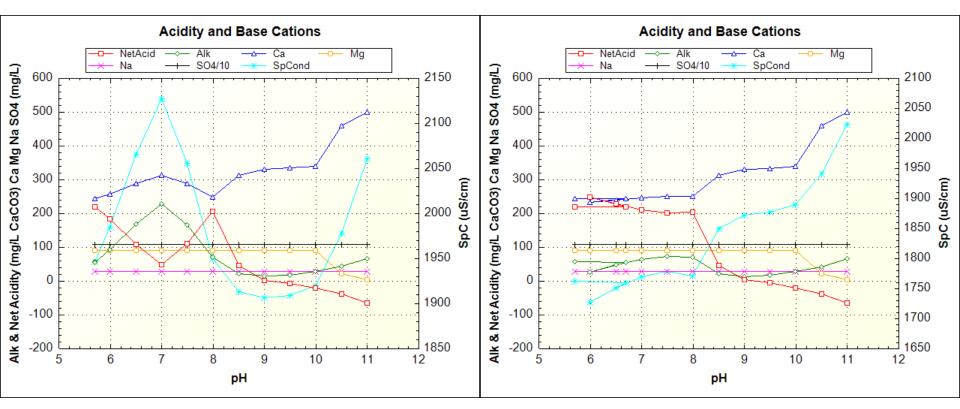
CausticTitration.exe: Pre-aerated (Graph1)



# Caustic Titration with Pre-Aeration (Decarbonation) St. Michael: pre-aeration decreases $CO_2$ acidity, caustic usage, and sludge

CausticTitration.exe: Not aerated (Graph2)

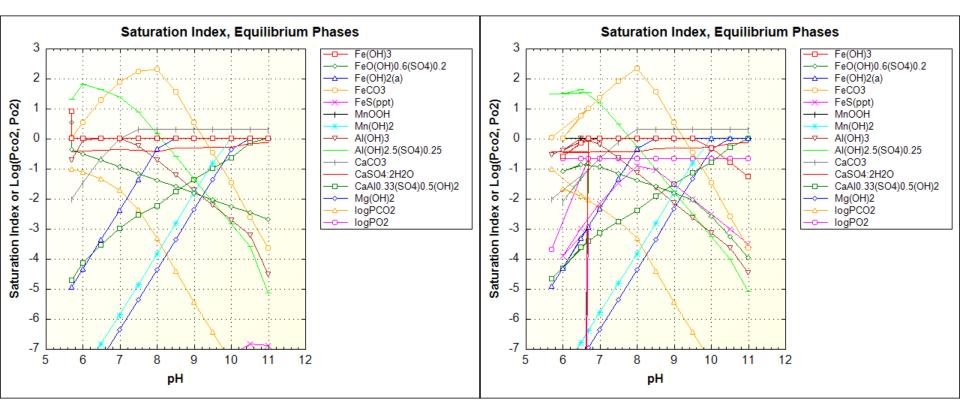
CausticTitration.exe: Pre-aerated (Graph2)



### Caustic Titration with Pre-Aeration (Decarbonation) St. Michael: pre-aeration decreases $CO_2$ acidity, caustic usage, and sludge

#### CausticTitration.exe: Not aerated (Graph3)

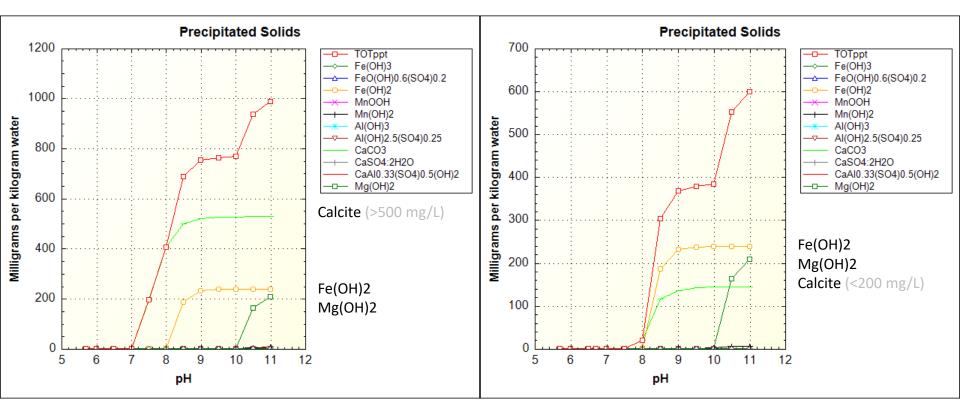
#### CausticTitration.exe: Pre-aerated (Graph3)



# Caustic Titration with Pre-Aeration (Decarbonation) St. Michael: pre-aeration decreases $CO_2$ acidity, caustic usage, and sludge

#### CausticTitration.exe: Not aerated (Graph4)

#### CausticTitration.exe: Pre-aerated (Graph4)



**pH** ≥ 8.5: Calcite > 500 mg/L pH ≥ 10.5: Mg(OH)2 > 100 mg/L **pH > 8.5: Calcite < 200 mg/L** pH **>** 10.5: Mg(OH)2 > 100 mg/L

Automatic scale change for Y axis

### PHREEQ-N-AMDTreat: Parallel & Sequential Models

					Kinetics C	onstants, i	Adju	stment Facto	<sup>ors</sup> Kir	netics (a	djustme	nt fact	or app	lied to	all steps)
		factr.kCO2		1	factr.k0	)2	2.1		EXPcc		0.67				sing (CO <sub>2</sub> /O <sub>2</sub> )
		factr.kFeHOM	I	1	factr.kF	eHET	1		0.25		on Oxid				
		factr.kFeH2O2	2	1	factr.kb	act	1		factr.kFe	IIMnOx	1			- microb	eterogeneous ial)
		factr.kMnHON	И	1	factr.kN	<b>I</b> nHFO	1		factr.kM	nHMO	0.5			se Oxida	
		factr.kSHFO		1	factr.kS	60C	100	)	factr.kD0	DC	1	0	rganic C	arbon C	xidation
		SI_CaCO3		0.3 ~	SI_AI(O	H)3	0.0	~	SI_Fe(O	H)3	0.0	V So	olids Pre	ecipitatio	on
		SI_FeCO3,Mn	CO3	2.5 ~	SI_Bas	aluminite	3.0	~	SI_Schw	vertmannite	1.0	<u>ب</u> (۱	saturati	on index	/equilibrium)
Caustic	⊢ lf a	dded at ste adding caustic Caustic checkb	at step 1, oox(es) an	, 2, 3, 4, and/or d enter target p a(OH)2 ON	H value for the	e step(s)	t, ac 20	tivate releva			I <sub>2</sub> O <sub>2</sub> estin ✓ Estima 1.52E-05	te H2O2.n		00177	II oxidation
		: Duration H? Time.hrs		Peroxide C H2O2.mol			-ten)		stone/Com	•	orbent N HMeO.m	•	mpositi Mn%	ion (foi Al%	r each step) Description
	7.5	6	15.1		0.00066	-3.4	auni) 	0		0	0	100	0	<b>N</b> <sup>1</sup> /•	Aer3
✓ 1:			15.1		0.00066	-5.4	_			<u> </u>	<u> </u>		U		
✓ 2:	Caustic A	ddition:		H <sub>2</sub> O <sub>2</sub> :	Outgassi			Limeston	ne / Organi	c Carbon:	Sorben	t (reciro	culated	solids):	Aer2
3:	Steps 1 - 5	5			Ingassing	;:		Surface an	rea (SAcc.cm	n2/mol)	Mass to	tal Fe+N	1n+Al (H	MeO.mg	Aer1
✓ 4:					Rate (kLaC	CO2.1/s)		Mass avai	ilable (M/M	Occ)	Compos	ition (%)	) Fe, Mn,	, and Al	Aer0
5:	Choose ca	ustic agent	j	factr.kFeH2O2	factr.kCO2			equilibriur	n approach (l	EXPcc)					H2O2
<b>6</b> :	Specify tar	get pH			factr.kO2			calcite sat	uration limit	(SI_CaCO3)					NULL
7:					steady-stat	te logPCO	2	Organic ca	arbon mass	available (	SOC.mol)				NULL
8:								factr.kSHF	O (reduction	of FeIII)					NULL
9:								factr.kSOC	C (solid organ	ic carbon)					NULL
<b>10</b> :								factr.kDO	C (dissolved o	rganic carbo	on)				NULL
11:		0	15.1	0	0	-3.4	$\sim$	0	1	0	0	0	0	0	NULL
															L

Generate Kinetics Output

Print PHREEQC Output Report

### PHREEQ-N-AMDTreat: "ParallelTreatment.exe"

Select folder f		•	<u> </u>		a\WestBranch		erationEvp		Oa	k Hil	ΙB	ore	nol	es (	Ju	ne-	Jul	y 2013)	)
One or two			and near_ge	ocalem_dat	a weetbrailtri		crationexp											, - ,	
initial solutions: Design flow (gpm)	Soln#A 4694	Soln#B				Г		-		Adjustment Fac	-			0.07	— К	inetic p	arame	ters use	
Mix fraction	1	0			factr.kCO2		•	factr.k		2.1		EXPcc		0.67				es" with	
Temp (C)	15.1	0.01			factr.kFeHOM		1	factr.k		1		factr.kFeNO3		0.25				actors for	
SC (uS/cm)	1280	0			factr.kFeH2O2			factr.kl		1		factr.kFellMn		1	a	djustm	ent.		
DO (mg/L)	1.6	0.01			factr.kMnHON	· L			MnHFO	1		factr.kMnHM	0	0.5					
рН	6.4	0			factr.kSHFO			factr.k		100		factr.kDOC		1					
Acidity (mg/L)	0	0			SI_CaCO3		0.3 ~	SI_AI(		0.0 ~	-	SI_Fe(OH)3		0.0	~				
Estimate NetAcidity	-107.8	0			SI_FeCO3,Mn	CO3	2.5 ~	SI_Bas	aluminite	3.0 ~		SI_Schwertm	lannite	1.0	~				
Alk (mg/L)	150	0			adding caustic Caustic checkb					t, activate relev	vant			🗹 Estima	ite H2O2.r	mol/L 0.0	00177	]	
TIC (mg/L as C)	0	0						la2CO3		20 ~ v	vt% soln			1.52E-05	35wt%	1.44E-05	5 50wt%	- - 2	
Estimate TIC	63.5	0				<b>T</b> 0.0								H2O2 wt%		2.			
Fe (mg/L)	19.7	0		austic ?>p	H? Time.hrs	Temp2.0	H2O2.mol	kLaCO2.1/s	-3.4	.atm) SAcc.cm	2/mol	M/MUCC :	SOC.mo	HMeO.m	g Fe%	Mn%	AI%	Description Aer3	
Fe2 (mg/L)	19.7	0		7.5	6	15.1	0	0.0008	-3.4	~ 0 ~ 0			_	0					
Estimate Fe2	0	0	☑ 2: [				0							0	100			Aer2	
Al (mg/L)	0.056	0	☑ 3: [	7.5	6	15.1	0	0.00010	-3.4	~ 0	1	0		0	100	0	0	Aer1	
Mn (mg/L)	3.6	0	☑ 4: [	7.5	6	15.1	0	0.000005	-3.4	~ 0	1	0	_	0	100	0	0	Aer0	
SO4 (mg/L)	400	0	<b>⊘</b> 5: [	7.5	6	15.1	0.00018	0.000005	-3.4	~ 0	1	0		0	100	0	0	H2O2	
Cl (mg/L)	7.9	0	6:		0	15.1	0	0	-3.4	~ 0	1	0		0	0	0	0	NULL	
Ca (mg/L)	79	0	□ 7 <b>[</b>	Para	Ilel: i	ndo	nenc	lent .	st01		2 5	ame	inf	luon	+ 1	nto	r ai	uality.	
Mg (mg/L)	64	0	8	uru		nue	penc	ieni .		JJ UJ(		ume	,	luch		ure	' 40	ianry.	
Na (mg/L)	31.6	0	9	Ini	able	not	ontio	n tim	100	tom	hon	atur	0	$\sim$		-000	cin	2	
K (mg/L)	1.74	0							-	•			-	_		-	•		
Si (mg/L)	5.72	0	1	ime	stone	e sui	rfac	e are	a, o	rgani	CC	arbo	on,	sort	oen <sup>.</sup>	t ma	<b>155</b>	and	
NO3N (mg/L)	0.1	0			positi					-									
TDS (mg/L)	0	0	C C	2011	positi	UN,	120	2, cu	usi	c, uu	Jus	nubl	CI	ure	Iu		5.		
DOC (mg/L as C)	0.1	0			Plot	Dis. Metals	F	lot Ca, Acidity		Plot Sat Ind	ex		ot PPT S	olids					
Humate (mg/L as C)	0.1	0								ParallelTrea	tment.e	ke created by	y C.A. Cra	avotta III, U	.S. Geolog	jical Surve	y. Versior	n 1.4.5, August 2021	

Cravotta, C.A. III, 2021. Interactive PHREEQ-N-AMDTreat water-quality modeling tools to evaluate performance and design of treatment systems for acid mine drainage: Applied Geochemistry, 126, 10845. https://doi.org/10.1016/j.apgeochem.2020.104845



### PHREEQ-N-AMDTreat: Parallel Model

Effects of O<sub>2</sub> Ingassing and CO<sub>2</sub> Outgassing on pH and Fe<sup>II</sup> Oxidation Rates

Batch Aeration Tests at Oak Hill Boreholes (summer 2013, 6-hour duration)

### **Control Not Aerated**

Aerated

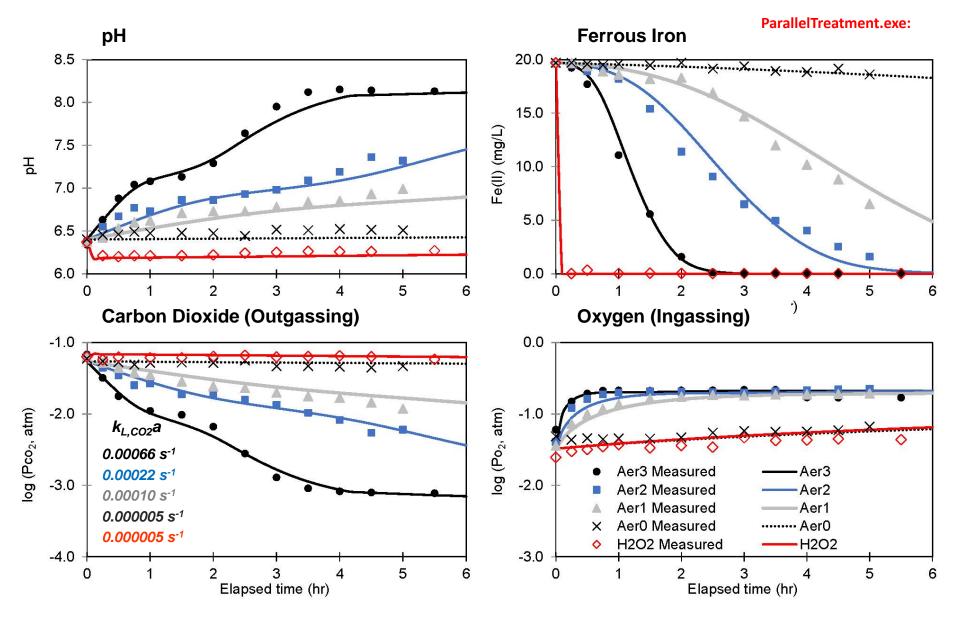
H<sub>2</sub>O<sub>2</sub> Addition



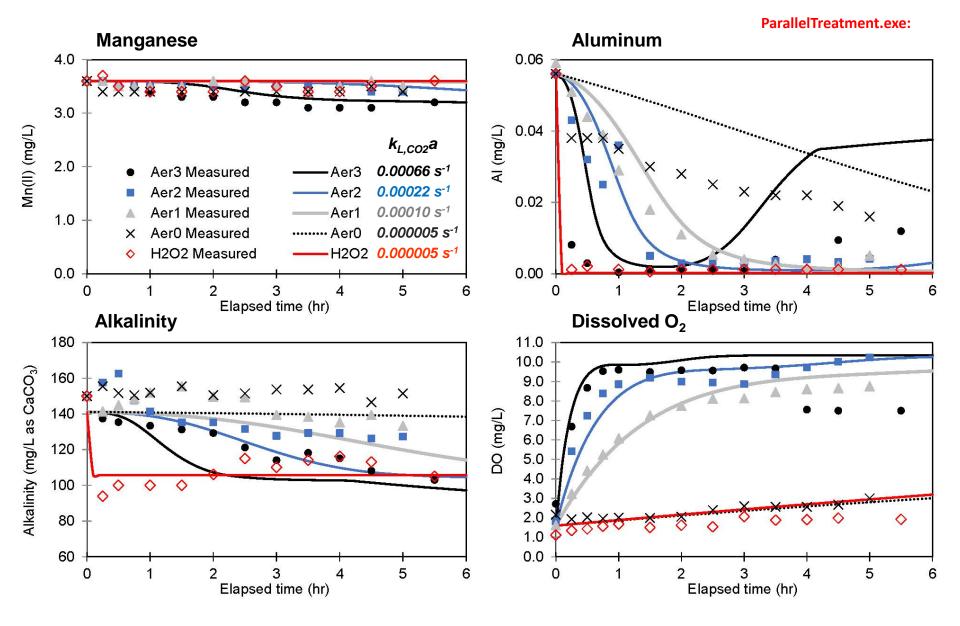




### PHREEQ-N-AMDTreat: Parallel Model Batch Aeration Tests at Oak Hill Boreholes

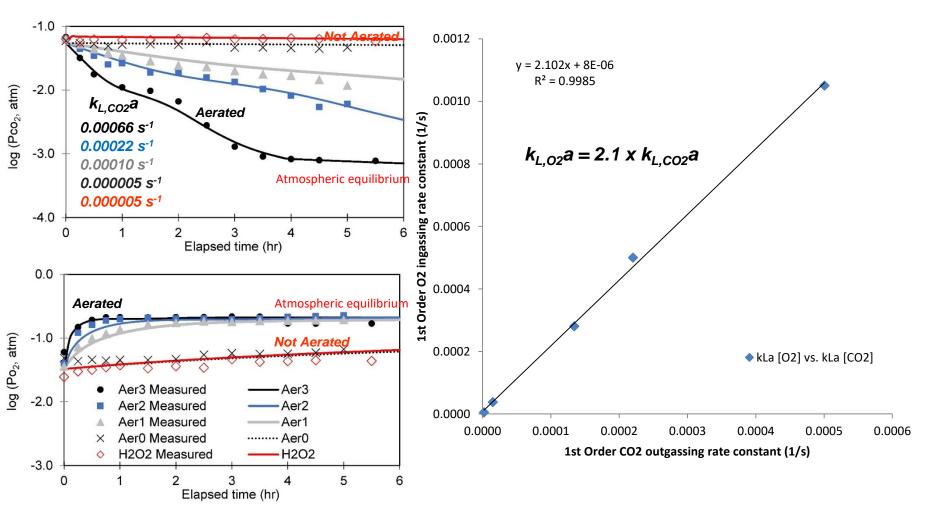


### PHREEQ-N-AMDTreat: Parallel Model Batch Aeration Tests at Oak Hill Boreholes



# $CO_2$ Outgassing is Proportional to $O_2$ Ingassing (model specifies first-order rates for out/in gassing)

 $-d[C]/dt = k_{L,C}a \cdot ([C] - [C]_S)$  exponential, asymptotic approach to steady state



### CO<sub>2</sub> Outgassing & O<sub>2</sub> Ingassing Rate Constants Estimated for Various Treatment Technologies

Table S2. Typical empirical values of rate constants for	for $CO_2$ out	gassing and	$O_2$ ingass	ing	
	Temper-	CO <sub>2</sub> Oι	utgas	O <sub>2</sub> Ing	as
Site	ature	k <sub>L,CO</sub>	<sub>2</sub> a	k <sub>L,02</sub>	а
	(°C)	(s <sup>-1</sup> )	log(s <sup>-1</sup> )	(s <sup>-1</sup> )	$\log(s^{-1})$
Treatment Systems					
Maelstrom (Sykesville, Trent, St.Michaels)	20 Fast	0.03	-1.52	0.063	-1.20
Surface Aerator (Renton, other)	20	0.001	-3.00	0.0021	-2.68
Mechanical Aerator (Lancashire)	20	0.0006	-3.22	0.00126	-2.90
Aeration Cascade/Level Spreader (Silver Cr)	20	0.01	-2.00	0.021	-1.68
Rip-rap Spillway/Ditch (Silver Cr, Pine Forest,	20	0.005	-2.30	0.0105	-1.98
Pond (Silver Cr, Pine Forest, Lion Mining, Flight93)	20	0.00001	-5.00	0.000021	-4.68
Wetland (Silver Cr, Pine Forest, Lion Mining)	20	0.00001	-5.00	0.000021	-4.68
Anoxic limestone drain (Pine Forest)	20 <mark>Slo</mark> v	v0.000001	-6.00	0.0000021	-5.68
Oak Hill Aeration Expts.					
Aer3	20 Fast	0.00066	-3.18	0.00139	-2.86
Aer2	20	0.00022	-3.66	0.00046	-3.34
Aer1	20	0.00010	-4.00	0.00021	-3.68
AerO	20 <mark>Slov</mark>	<mark>v</mark> 0.000005	-5.30	0.000011	-4.98
AerO	0.000			a toy to so of a contract to the annual so	-4.98

\*Gas mass-transfer rate corrected to 20°C per Rathbun (1998, Eq. 56) using the expression:

kL,a\_20 = kL,a\_TC /(1.0241^(TC-20)).

kL,a\_TC = kL,a\_20 \* (1.0241^(TC-20)).

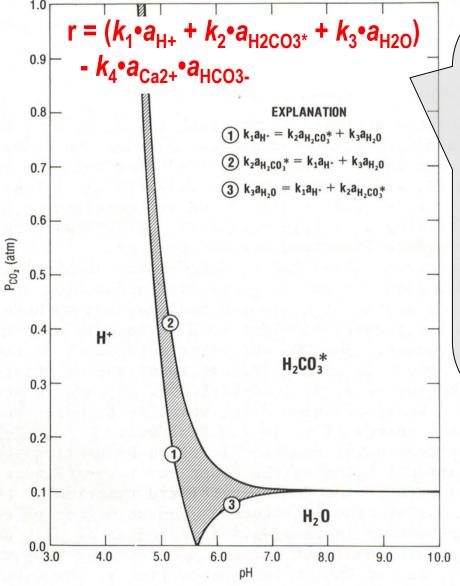


kL,a\_20 =  $(LN((C_1-C_s)/(C_2-C_s))/t) / (1.0241^{(TEMPC - 20)})$ , where C is CO<sub>2</sub> or O<sub>2</sub>. Dissolved O<sub>2</sub>, temperature, and pH were measured using submersible electrodes. Dissolved CO<sub>2</sub> was computed from alkalinity, pH, and temperature data.

# KINETICS OF LIMESTONE DISSOLUTION – pH, CO<sub>2</sub>, and SURFACE AREA EFFECTS



### Limestone Dissolution Rate Model for AMDTreat ("PWP" model emphasizes pH and CO<sub>2</sub>)



According to Plummer, Wigley, and Parkhurst (1978), the rate of  $CaCO_3$ dissolution is a function of three forward (dissolution) reactions:  $CaCO_3 + H^+ \rightarrow Ca^{2+} + HCO_3^$  $k_1$  $CaCO_3 + H_2CO_3^* \rightarrow Ca^{2+} + 2 HCO_3^$  $k_2$  $CaCO_3 + H_2O \rightarrow Ca^2 + HCO_3 + OH^2$  $k_3$ and the backward (precipitation) reaction:  $Ca^{2+} + HCO_{3-} \rightarrow CaCO_{3} + H^{+}$ K₄

Although H<sup>+</sup>,  $H_2CO_3^*$ , and  $H_2O$  reaction with calcite occur simultaneously, the forward rate is dominated by a single species in the fields shown. More than one species contributes significantly to the forward rate in the gray stippled area. Along the lines labeled 1, 2, and 3, the forward rate attributable to one species balances that of the other two.

### Limestone Dissolution Rate Model for AMDTreat (surface area correction for coarse aggregate)

Surface area for various coarse aggregates (bold indicates sizes commonly used in limestone beds; 2NS used in cubitainers).

Gradation	Number	Weight (g)	Pa	rticle Dime	nsions (c	m)	Particle S	urface Ar	ea (cm^2)	Unit Surface Area (cm^2/g)				
AASHTO	PA	Average Particle	Long Axis	Inter- mediate	Short Axis	Average Axis	Rectan- gular Prism	Sphere	Ellipsoid	Rectan- gular Prism	Sphere	Ellipsoid		
R-5		22160.145	45.72	22.86	13.34	27.31	3919.35	2342.26	2862.08	0.18	0.11	0.13		
R-4		7113.133	30.48	16.51	8.89	18.63	1841.93	1089.98	1319.11	0.26	0.15	0.19		
R-3		1185.522	16.51	8.89	5.08	10.16	551.61	324.29	395.61	0.47	0.27	0.33		
1	4	341.978	8.89	6.35	3.81	6.35	229.03	126.68	155.24	0.67	0.37	0.45		
3	3A	78.166	5.08	3.81	2.54	3.81	83.87	45.60	56.39	1.07	0.58	0.72		
5		9.771	2.54	1.91	1.27	1.91	20.97	11.40	14.10	2.15	1.17	1.44		
57	2B	3.257	2.54	1.27	0.635	1.48	11.29	6.90	8.25	3.47	2.12	2.53		
	2NS	9.771	2.54	1.91	1.27	1.91	20.97	11.40	14.10	2.15	1.17	1.44		
67	2	1.832	1.91	0.95	0.635	1.16	7.26	4.26	5.28	3.96	2.32	2.88		
	1NS	1.221	1.27	0.95	0.635	0.95	5.24	2.85	3.52	4.29	2.33	2.89		
7		1.221	1.27	0.95	0.635	0.95	5.24	2.85	3.52	4.29	2.33	2.89		
8		0.382	0.95	0.79	0.3175	0.69	2.62	1.49	1.70	6.87	3.90	4.44		
	1B	0.382	0.95	0.79	0.3175	0.69	2.62	1.49	1.70	6.87	3.90	4.44		

Particle dimensions were estimated on the basis of ranges for graded materials reported in Pennsylvania Department of Environmental Protection, 2000, Erosion and sediment pollution control program manual: Harrisburg, Pennsylvania Dept. Environmental Protection Bureau of Watershed Management, Document No. 363-2134-008, 180 p. (tables 9 and 10A).

Plummer, Wigley, and Parkhurst (1978) reported unit surface area (SA) of 44.5 and 96.5 cm<sup>2</sup>/g for "coarse" and "fine" particles, respectively, used for empirical testing and development of PWP rate model. These SA values are 100 times larger than those for typical limestone aggregate. *Multiply cm<sup>2</sup>/g by 100 g/mol to get surface area (A) units of cm<sup>2</sup>/mol used in AMDTreat rate model.* 

Surface area computed for various geometric forms:

Sphere: 4pi\*(Average of Axes/2)^2

Rectangular Prism: 2\*(Long Axis\*Short Axis)+2\*(Long Axis\*Intermediate Axis)+2\*(Short Axis\*Intermediate Axis)

Ellipsoid:  $(pi*D^2)/S$ , where  $D=2*(vol/(4/3pi))^{(1/3)}$ 

S=1.15-0.25E

E=Long Axis/D

Volume computed for same geometric forms:

Sphere: 4/3\*pi\*(Average Axis/2)^3

Rectangular Prism: (Long Axis\*Short Axis\*Intermediate Axis)

Ellipsoid: 4/3\*pi\* (Long Axis/2\*Short Axis/2\*Intermediate Axis/2)

For ellipsoid sphere, this reduces to 0.5236\*Long Axis\*Short Axis\*Intermediate Axis

Santomartino and Webb (2007, AG, 22:2344-2361) estimated volume of ellipsoid as 0.6\*volume of rectangular prism of same dimensions.

### PHREEQ-N-AMDTreat "TreatTrainMix2.exe":

Select folder fo	older for input/output water-quality			Tre	eatTrai	i <b>nM</b> i	ix2.exe	e Seq	uen	tia	l Mod	lel	of	Succe	ssive	Trea	atme	ent S	teps (1-11)
	\Users\cravotta	Nocuments\A	MDTreat_geo	chem_data	a\WestBranch\	OAK+PK	N												
One or two	Soln#A	Soln#B						Kinetics C	onstants.	Adius	stment Facto	rs							ters use
initial solutions: Design flow (gpm)	2830	8976			factr.kCO2		1	factr.k0	12	2.1		F	EXPcc		0.67				es" with actors for
Mix fraction	0.24	0.76			factr.kFeHOM		1	factr.kF		1			actr.kFe	NO3	0.25		djustme		
Temp (C)	14.7	10.9			factr.kFeH2O2	2	1	factr.kb		1			actr.kFe		1		ajastin		
SC (uS/cm)	1000	570			factr.kMnHOM		1		<b>InHFO</b>	1			actr.kMr		0.5				
DO (mg/L)	2	9.9			factr.kSHFO		1	factr.ks		100	)		actr.kD0		1				
pН	6.3	6.4			SI_Fe(OH)3		0.0 ~	SI_AI(O	)H)3	0.0	~		GI_CaCC		0.3	~	Solids I	Precipi	tation
Acidity (mg/L)	-111	-20			SI_Schwertma	nnite	1.0 ~	SI_Bas	aluminite	3.0	~	S	SI_FeCO	3,MnCO3	2.5	~	(SI=0 is	s equili	brium)
Estimate NetAcidity	-110.6	-19.9	Optio	on to ad	ld specified	d caust	ic agent to	o adjust pl	H at be	gini	ning of st	eps	1-5:						
Alk (mg/L)	150	34			adding caustic Caustic checkb					nt, act	tivate relevar	nt			🗹 Estima	te H2O2.r	nol/L 7.4	E-05	
TIC (mg/L as C)	0	0			🔿 CaO		(OH)2 O N			20	∼ wt	soln 🖁			6.4E-06		6E-06	50wt%	
🗹 Estimate TIC	73.3	15.7	Step +Ca	austic?>p	H? Time.hrs	Temp2(	C H2O2.mol	kL=CO21/a		(atm)	SAcc cm2/	nol M	1/M0ee	500 mg	HDOD4%	unto gou	<del>gal (meme</del> Mn%	Al%	Description
Fe (mg/L)	18	5.15		7.5	0.25	14.7		0.000005	-3.4		0			0	0	100	0	0	Sedimentation pond
Fe2 (mg/L)	18	5.15	☑ 1: [	7.5	0.05	14.7	0.000074	0.005	-3.4		0	」( <u> </u>			0	100		0	H2O2+Mixing
Estimate Fe2	0	0	☑ 2:							_									-
AI (mg/L)	0.06	0.07	☑ 3:	7.5	4	15.1	0	0.000005	-3.4	=	0	1		0	3	99.8	0.1	0.1	Oxidation/settling pond
Mn (mg/L)	3.7	2.45	☑ 4: [	7.5	0.01667	15.1	0	0.005	-3.4	~	33			0	2	99.8	0.1	0.1	Aeration riprap
SO4 (mg/L)	390	240		7.5	1	15.5		0.000005	-3.4	~	144			<b>TO#</b> 5	2	95	5	0	Aerobic wetland
Cl (mg/L)	8.8	17.5	<b>⊠</b> 6:		0.0333	15.5	0	0.005	-3.4	~	33		R-3		2	95	5	0	Aeration riprap
Ca (mg/L)	99	40.5	7:		0.5	16	0	0.0005	-3.4	~	72			<b>T</b> O#3	20	10	90	0	Mn removal bed
Mg (mg/L)	55	42	8:		0.01667	17	0	0.005	-3.4	~	33	1	R-3	0	1	100	0	0	Ditch
Na (mg/L)	32	10	9:	Sea	uenti	al '	Varia	hle r	ete	n	tion	tir	ne	s te	mne	rat	ure	H	$\mathbf{O}_{\mathbf{a}}$
K (mg/L)	1.74	1.77		•										-	•			-	
Si (mg/L)	5.72	5.72			stic, (										ace	arec	1, OI	rgai	าเด
NO3N (mg/L)	0.1	0.1		cart	oon, s	ort	oent.	plus	adi	us	stab	e	rat	tes.					
TDS (mg/L)	0	0			••••			F	J			_							
DOC (mg/L as C)	0.1	0			Plot [	Dis. Metal	s P	lot Ca, Acidity		P	lot Sat Index			Plot PPT	Solids				
Humate (mg/L as C)	0.1	0								Т	reat Train Mix2	2.exe (	created	by C.A. Crav	votta III, U.S.	Geologica	al Survey.	Version 1	.4.5, August 2021

Cravotta, C.A. III, 2021. Interactive PHREEQ-N-AMDTreat water-quality modeling tools to evaluate performance and design of treatment systems for acid mine drainage: Applied Geochemistry, 126, 10845. https://doi.org/10.1016/j.apgeochem.2020.104845

### PHREEQ-N-AMDTreat: TreatTrainMix2 Model Pine Forest ALD\* + Pond + Aerobic Wetlands



<u>Step</u> 0 1 2	<u>Treatment</u> Untreated ALD Riprap
3	Pond
4	Riprap
5	Wetland
6	Cascade
7	Wetland
8	Cascade
9	Wetland
10	Riprap
11	NULL

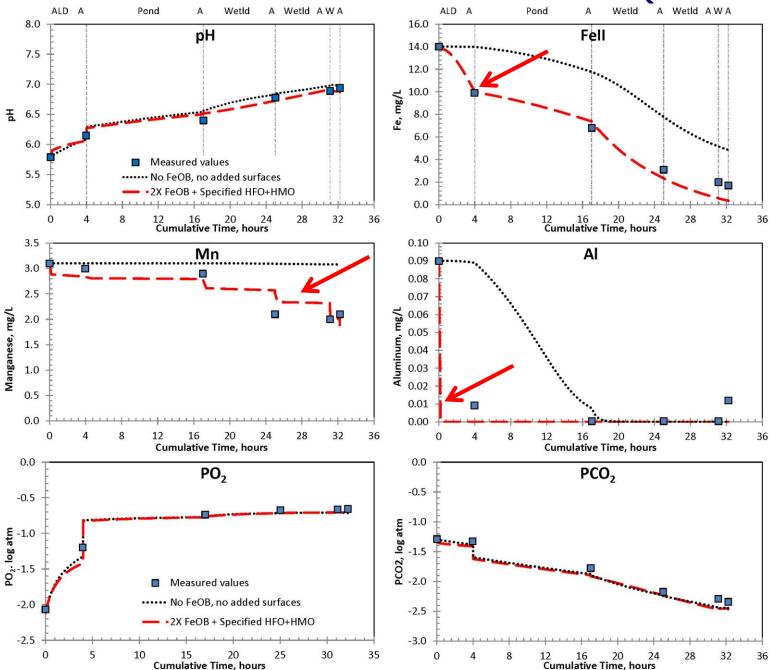
#### \*Flushable ALD, Biofouled

## PHREEQ-N-AMDTreat: TreatTrainMix2 Model

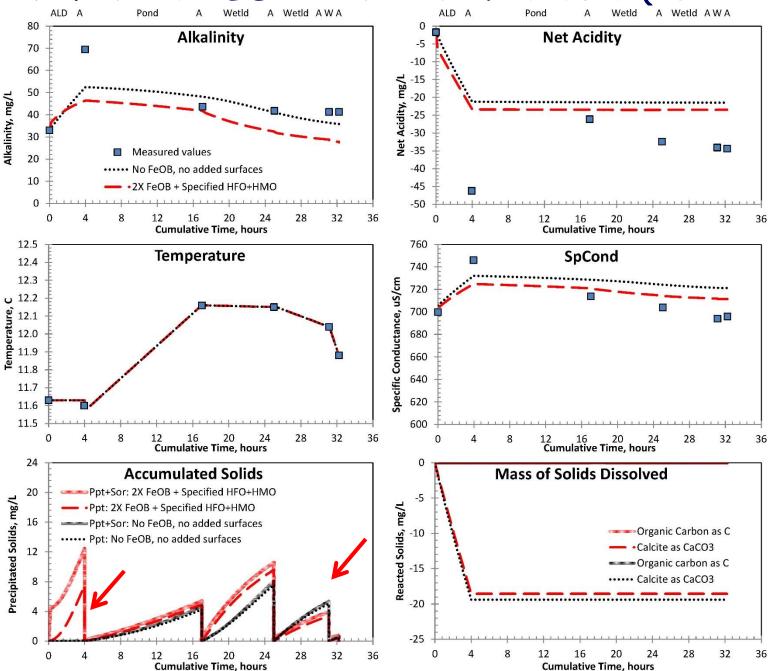
TreatTra						-		Bic	foi	ıl,	ed A	ID-	Aer	obic	Po	nd-	+W/	etlands
TreatTrainMix2.exe:       Passive treatment         t Workspace       C:\Users\cravotta\Documents\AMDTreat_geochem_data\MillCreek\PineForestLowerTreatment       Biofouled ALD+Aerobic Pond+Wetlands         Soln#A       Soln#B       Kinetics Constants, Adjustment Factors       Pine Forest (151212)																		
	Soln#A	Soln#B						Kinetics	Constants,	Adju	stment Factor	s		Ine	10	res	† (J	(51212)
esign flow (gpm)	690	0			factr.kCO2		1	factr.k	02	2.1		EXPco	;	0.67				
lix fraction	1	0			factr.kFeHOM		1	factr.k	FeHET	1		factr.k	FeNO3	0.25				
emp (C)	11.63	0.01			factr.kFeH2O2	2	1	factr.k	bact	2		factr.k	FellMnOx	1				
C(uS/cm)	700	0	_		factr.kMnHOM	1	1	factr.k	MnHFO	1		factr.k	MnHMO	0.5				
)O (mg/L)	0.4	0.01			factr.kSHFO		1	factr.k	SOC	100	)	factr.k	DOC	5				
н	5.79	0			SI_Fe(OH)3		0.0	SI_AI(	DH)3	0.0	~	SI_Ca	003	0.3	$\sim$			
cidity (mg/L)	0	0			SI_Schwertma	innite	1.0	✓ SI_Ba:	aluminite	3.0	~	SI_Fe	CO3,MnCO3	2.5	$\sim$			
Estimate NetAcidity	-1.7	0																
lk (mg/L)	33	0			adding caustic Caustic checkb					nt, ac	tivate relevan	t		🗹 Estima	te H2O2.r	nol/L 0.0	00126	
TC (mg/L as C)	0	0			⊖ CaO	(он)2 О	○ Na2CO3 ○ NaOH 20 → wt% soln						1.08E-05		1.02E-05			
Estimate TIC	39.2	0	0	C	UD T 1	т ос		LL-002.1/	1_(000)		CA		505			-	), not used)	
e (mg/L)	14	0		-Caustic ?>p	H? Time.hrs	11.63	C H2O2.mo	kLaCO2.1/s	Lg(PCO2	atm)	72		c SOC.mo	HMeO.m	g Fe%  99	Mn%	AI%	Description
e2 (mg/L)	14	0	☑ 1:		4					_		 		110				
Estimate Fe2	0	0	✓ 2:	7.5	0.0083	11.6	0	0.02	-3.4	_	33		0		95	5	0	Aeration riprap
l (mg/L)	0.09	0	<b>⊘</b> 3:	7.5	13	12.16	0	0.00002	-3.4	_	0	1	0	3	95	5	0	Oxidation/settling pond
In (mg/L)	3.1	0	✓ 4:	7.5	0.0028	12.16	0	0.005	-3.4	~	0	1	0	1	95	5	0	Aeration cascade
04 (mg/L)	330	0	<b>⊘</b> 5:	7.5	8	12.15	0	0.00005	-3.4	~	0	1	0.1	3	60	40	0	Aerobic wetland
1 (mg/L)	4	0	<b>⊘</b> 6:		0.0028	12.15	0	0.005	-3.4	$\sim$	0	1	0	1	60	40	0	Aeration riprap
a (mg/L)	56	0	7:		6.1	12.04	0	0.00005	-3.4	$\sim$	0	1	0.1	2	40	60	0	Aerobic wetland
lg (mg/L)	51	0	8:		0.0028	12.04	0	0.005	-3.4	$\sim$	0	1	0	1	40	60	0	Aeration riprap
la (mg/L)	7.4	0	<b>⊘</b> 9:		1.1	11.88	0	0.00001	-3.4	$\sim$	0	1	0.1	2	20	80	0	Aerobic wetland
(mg/L)	0.54	0	✓ 10:		0.0042	11.88	0	0.005	-3.4	~	0	1	0	1	20	80	0	Aeration riprap
i (mg/L)	5.4	0	11:		0	11.88	0	0	-3.4	$\sim$	0	1	0	0	100	0	0	NULL
IO3N (mg/L)	1.5	0																
DS (ma/L)	450	0					1	Gene	rate Kineti	cs Ou	itput	1		D Pr		EQC Outpu	t Depert	
03 (mg/L) 10C (mg/L as C)	3.67	0				Dis. Metal		Plot Ca, Acidity			lot Sat Index	-				lac outpu	rneport	
		0				Dist metal	• L	FIOL Ca, ACIDILY										
lumate (mg/L as C)	0.67	U								Т	reatTrainMix2	.exe create	ed by C.A. Cra	votta III, U.S	. Geologica	al Survey.	Version 1	.4.5, August 2021

Variable retention times, temperature, (caustic,  $H_2O_2$ ,)  $CO_2$  outgassing/ingassing, limestone surface area, organic carbon, sorbent, plus adjustable rates.

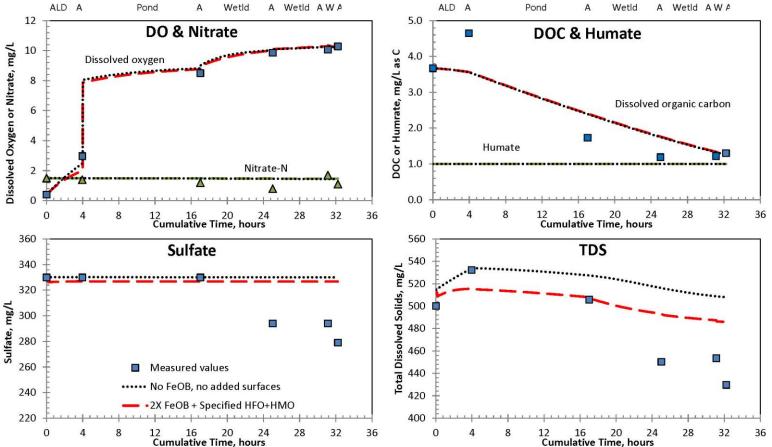
### Pine Forest ALD + Aerobic Wetlands (151212)



#### Pine Forest ALD + Aerobic Wetlands (151212)



Pine Forest ALD + Aerobic Wetlands (151212)

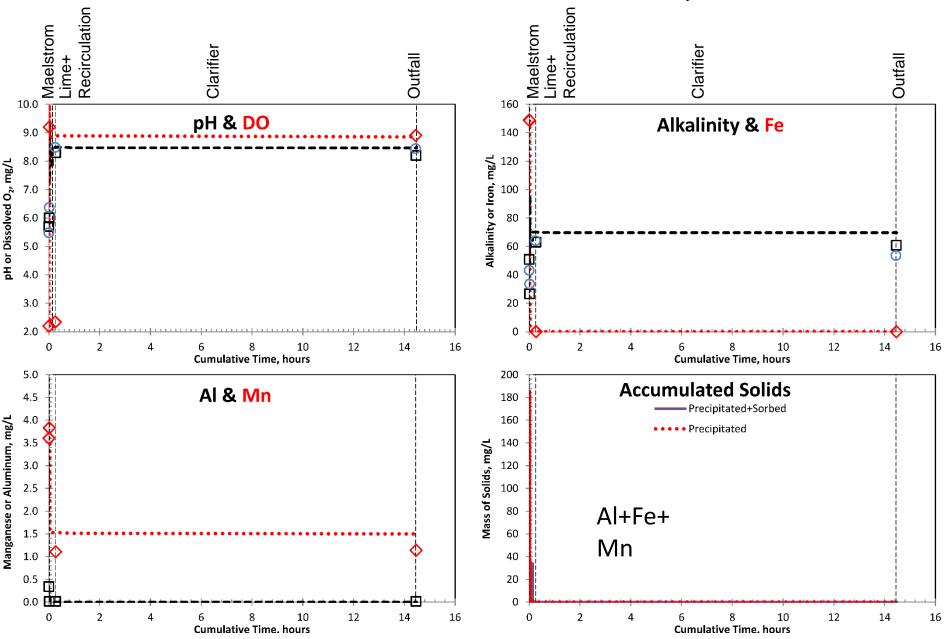


## Pre-Aeration, Lime Dosing, Solids Recirculation

TreatTrai	nMix2	.exe: A	ctiv	e tre	atment									C	5+	Mid	ha	el AMD:		
Select Workspace	ace C:\Users\cravotta\Documents\AMDTreatTrainREYs_wateq\StMichael																			
	Soln#A	Soln#B	Kinetics Constants, Adjustment Factors net acidic with																	
Design flow (gpm)	5200	0			factr.kCO2		1 factr.kO2 2.1 EXPcc							0.67	D.67 biob Eo & CO					
Mix fraction	1	0			factr.kFeHOM	1	1	factr.kFeHET 1 factr.kFeNC				eNO3	<sup>0.67</sup> <sub>0.25</sub> high Fe & CO <sub>2</sub>							
Temp (C)	15.4	0.01			factr.kFeH20	2	1	factr.kbact 1			factr.kF	ellMnOx	1	📃 moderate M						
SC (uS/cm)	1923	0			factr.kMnHOI	M	1	factr.kl	MnHFO	1		factr.kN	InHMO	0.5		THC.				
DO (mg/L)	2.2	0.01	1		factr.kSHFO		1	factr.ks	SOC	100		factr.kE	OOC	1						
pН	5.7	0			SI_Fe(OH)3		0.0	SI_AI(C	DH)3	0.0	~	SI_CaC	:03	2.5	~					
Acidity (mg/L)	254.2	0			SI_Schwertma	annite	1.0	✓ SI_Bas	aluminite	3.0	~	SI_FeC	O3,MnCO3	2.5	~					
Estimate NetAcidity	223	0																_		
Alk (mg/L)	50.8	0	If adding caustic at step 1, 2, 3, 4, and/or 5: choose caustic agent, activate relevant +Caustic checkbox(es) and enter target pH value for the step(s)															]		
TIC (mg/L as C)	57.3	0			● CaO	⊖ Ca	(OH)2 O	H)2 ONa2CO3 ONaOH 20 vt% soln							0.0001143 35wt% 0.0001082 50wt%					
Estimate TIC	63.5	0	H2O2 wt% units gal/gal (memo, not used) Step +Caustic?->pH? Time.hrs Temp2.C H2O2.mol kLaCO2.1/s Lg(PCO2.atm) SAcc.cm2/mol M/M0cc SOC.mo HMeO.mg Fe% Mn% Al% Description													l) Description				
Fe (mg/L)	148	0	1 · ·	-causic -	0.015	16.1		0.05	-3.4		0			nme0.m	g re~	0	0	Maelstrom (54 sec)		
Fe2 (mg/L)	148	0	☑ 1:		0.015	16.1		0.0001	-3.4		0	1		0	100			Lime Fe(OH)2 ppt equil		
Estimate Fe2	0	0	2:	8.5				0.0001	-3.4			<u>'</u>   1		227.7	97.51					
Al (mg/L)	0.34	0	<b>⊘</b> 3:	9.3	0.110	18.4					0					1.95	0.53	Lime+Solids Fe(OH)3 ppt		
Mn (mg/L)	3.6	0	<b>⊘</b> 4:	8.5	0.110	18.4	0	0.0001	-3.4		0	1	0	0	97.51	1.95	0.53	Lime pH 8.4 effl to clarifier		
SO4 (mg/L)	1078	0	<b>⊘</b> 5:	7.5	14.20	18.9	0	0.0000001	-3.4		0	1	0	1.7	100	0	0	Clarifier 4.43 Mgal		
Cl (mg/L)	32.8	0	<b>⊘</b> 6:		0.03	19.5	0	0.0005	-3.4		0	1	0	0	100	0	0	Outflow ditch		
Ca (mg/L)	242	0	7:		0	19.5	0	0	-3.4	$\leq$	0	1	0	0	100	0	0	NULL		
Mg (mg/L)	88.7	0	8:		0	15.4	0	0	-3.4	_	0	1	0	0	0	0	0	NULL		
Na (mg/L)	27.8	0	<b>⊘</b> 9:		0	15.4	0	0	-3.4	~ [	0	1	0	0	0	0	0	NULL		
K (mg/L)	9.15	0	✓ 10	):	0	15.4	0	0	-3.4	~ [	0	1	0	0	0	0	0	NULL		
Si (mg/L)	18.8	0	✓ 11	:	0	15.4	0	0	-3.4	~	0	1	0	0	0	0	0	NULL		
NO3N (mg/L)	0	0																		
TDS (mg/L)	0	0						Gene	rate Kineti	cs Out	put			Pri	nt PHRE	EQC Outpu	it Report			
DOC (mg/L as C)	0.1	0			Plot	Dis. Meta	ls 🗌	Plot Ca, Acidity		Plo	ot Sat Index	[	Plot PPT	Solids						
Humate (mg/L as C)	0.1	0								Tre	eatTrainMix2	exe create	d by C.A. Crav	votta III, U.S.	Geologic	al Survey.	Version 1	I.4.5, August 2021		

UI for active treatment of net-acidic AMD through (1) Maelstrom oxidizer; (2-4) lime dosing and sludge recirculation; (5) clarifier; and (6) outflow ditch.

#### Pre-Aeration, Lime Dosing, Solids Recirculation St. Michael AMD, Cambria County, PA



### PHREEQ-N-AMDTreat: TreatTrainMix2 Model Application

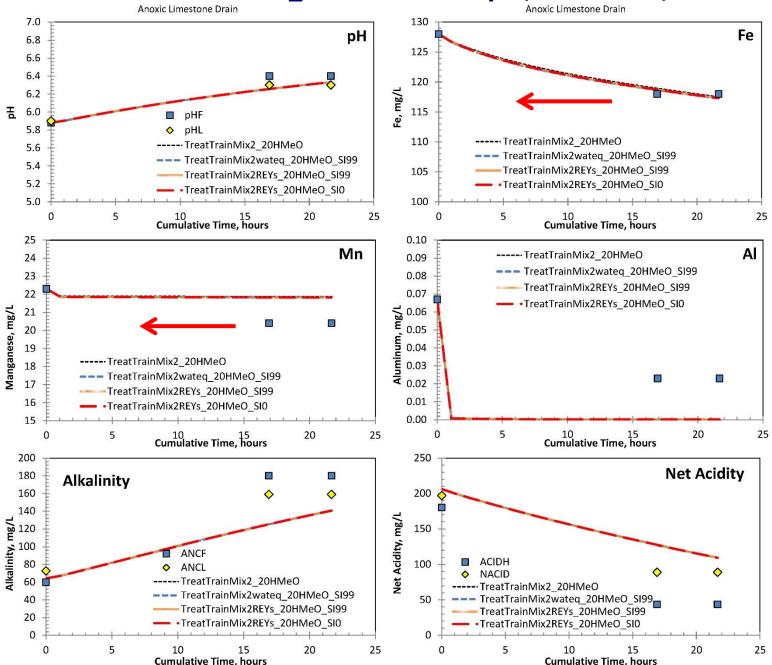
Hypothetical Passive Treatment Scenarios for Howe Bridge Mine Discharge

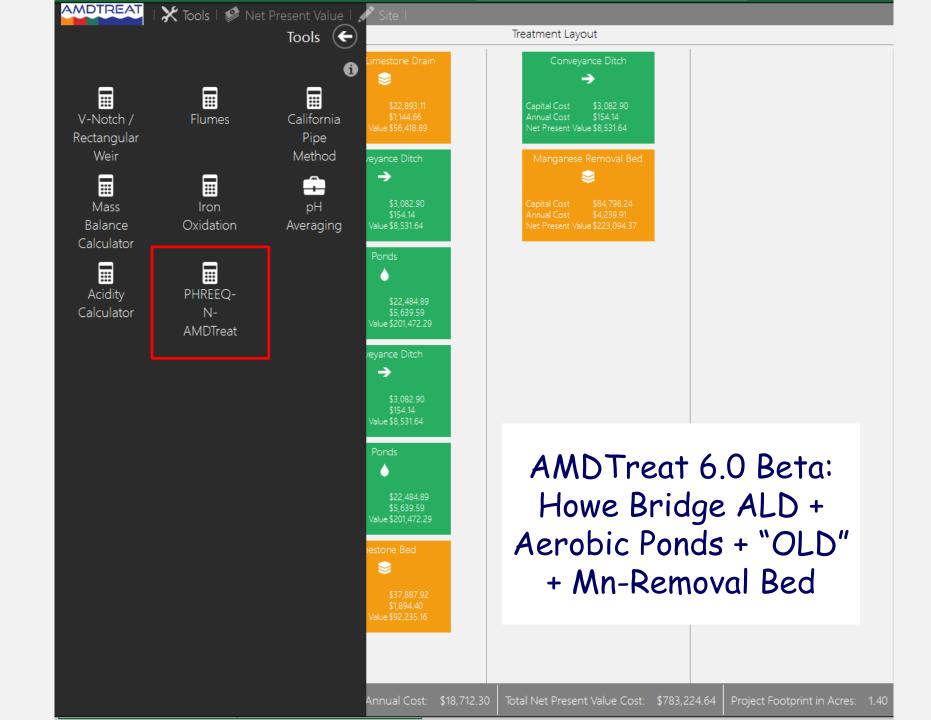
### "ALD" + Aerobic Ponds + "OLD" + Mn-Removal Bed

TreatTra	eatTrainMix2.exe: Passive treatment													ne	hia	h F	e & Mn
elect Workspace C:	C:\Users\cravotta\Documents\AMDTreatValidationSimulations\HOWBRALD       Howe Bridge, high Fe & Mn																
	Soln#A	Soln#B	Kinetics Constants, Adjustment Factors														
Design flow (gpm)	16.1	0		factr.kCO2		1	factr.k0	02	2.1		EXPcc		0.67				
Mix fraction	1	0		factr.kFeHOM		1	factr.kf	FeHET	1		factr.kF	eNO3	0.25				
Temp (C)	11.3	0.01		factr.kFeH2O2		1	factr.kb	bact	1		factr.kF	ellMnOx	1				
SC (uS/cm)	1270	0	_	factr.kMnHOM		1	factr.kMnHFO		1		factr.kMnHMO		0.5				
DO (mg/L)	1.12	0.01		factr.kSHFO		1	factr.ks	SOC	100	)	factr.k[	DOC	1				
pН	5.88	0		SI_Fe(OH)3		0.0 ~	SI_AI(OH)3		0.0	~			0.3 ~				
Acidity (mg/L)	180	0		SI_Schwertma	innite	1.0 ~	SI_Bas	aluminite	1.0	~	SI_FeC	O3,MnCO3	2.5	~			
Estimate NetAcidity	210.5	0					-										
Alk (mg/L)	60	0		<ul> <li>If adding caustic</li> <li>+Caustic checkb</li> </ul>				nt, ac	tivate releva	nt		🗹 Estima		mol/L 0.0		]	
TIC (mg/L as C)	32.4	0		a(OH)2 ONa2CO3 ONaOH 20 vt% sc							9.89E-05		9.36E-05				
🗹 Estimate TIC	58.8	0	Step +Caustic?-	mol M/M0c	c SOC.mo	H2O2 wt% HMeO.m		/gal (memo Mn%	, not used Al%	d) Description							
Fe (mg/L)	128	1E-08	· ·	21.7	9.8	0		-3.4		72		0	19.8	19 Pe %	16.0	0	ALD Howe Bridge 300
Fe2 (mg/L)	129	0		0.05	12		0.01	-3.4	~	45	1		0	100			Aeration cascade
Estimate Fe2	128	0	2:					-3.4	_		]['		-				
Al (mg/L)	0.067	1E-08	3:	20.0	12	0	0.00001			0			0	100			Aerobic pond
Mn (mg/L)	22.3	1E-08	☑ 4: □	0.05	12	0	0.01	-3.4		45		0	0	100	0	0	Aeration cascade
SO4 (mg/L)	684	1E-06	5:	40.0	12	0	0.0000001	-3.4		45		0	20	84.0	16.0	0	Limestone bed
Cl (mg/L)	4.9	0	<b>6</b> :	0.05	12	0	0.005	-3.4	~	45	1	0	0	100	0	0	Aeration cascade
Ca (mg/L)	101	1E-06	7:	8.0	12	0	0.00001	-3.4	~	0	1	0	0	100	0	0	Aerobic pond
Mg (mg/L)	63	1E-06	8:	0.05	12	0	0.01	-3.4	~	45	1	0	0	100	0	0	Aeration cascade
Na (mg/L)	12.2	1E-06	9:	5.0	12	0	0.0000001	-3.4	~	144	1	0	50	0	100	0	Mn removal bed
K (mg/L)	5.24	0	✓ 10:	5.0	12	0	0.0000001	-3.4	$\sim$	144	1	0	50	0	100	0	Mn removal bed
Si (mg/L)	7.05	0	✓ 11:	5.0	12	0	0.0000001	-3.4	$\sim$	144	1	0	50	0	100	0	Mn removal bed
NO3N (mg/L)	0	0															
TDS (mg/L)	1150	0					Gener	rate Kineti	cs Oi	utput			Pr	int PHRE	EQC Outpu	rt Report	
DOC (mg/L as C)	0	0		Plot	Dis. Metals	s 🗌 Pl	ot Ca, Acidity		P	lot Sat Index		Plot PPT	Solids				
Humate (mg/Las C)	0	0							-					Carles	10		4.5 August 2021

UI for passive treatment of net-acidic AMD through (1) anoxic limestone drain; with added steps for (3) aerobic pond; (5) oxic limestone bed; (7) aerobic pond; and (9,11) managenesis removal bed with intermediate ceretion steps (2, 4, 6, 8)

#### Howe Bridge ALD, only (210608)





#### "ALD" + Aerobic Ponds + "OLD" + Mn-Removal Bed

#### AMDTreat 6.0 Beta PHREEQ-N-AMDTreat tool:

#### Howe Bridge, high Fe & Mn

#### 📱 🏽 PHREEQ-N-AMDTreat | 🖍 Model Input | 🕕 Errors |

- -

Treatment Modules To Be Modeled

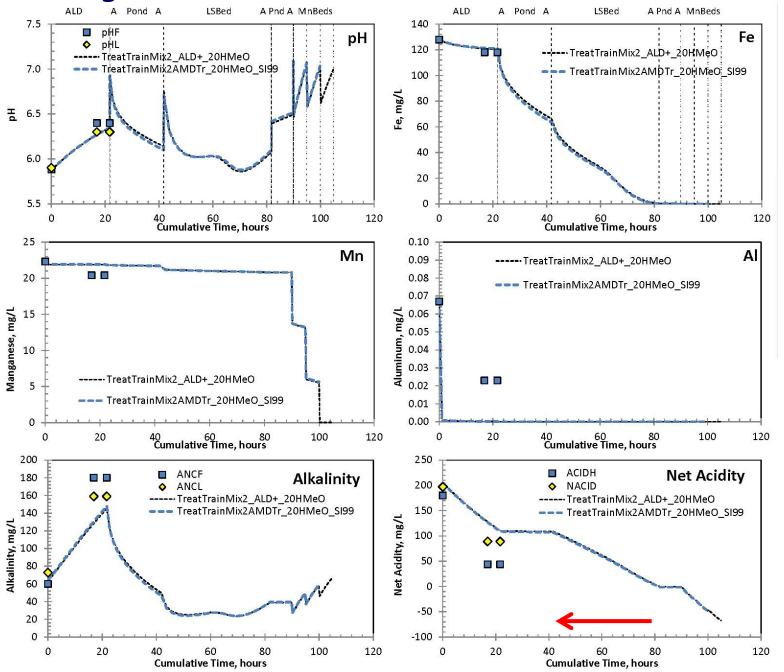
Treatment Module	Step	Treatment Layer/ Technology	Treatment pH (s.u.)	Retention Time (hrs)	Temperature (°C)	Decarbonation Rate: kLaCO <sub>2</sub> (sec <sup>-1</sup> )	Limestone Surface Area (cm²/mol)	Fraction of Limestone Available To React	Solid Organic Carbon	Sorbent Mass (Fe+Mn+Al) (mg/L)	Fe %	Mn %	<b>AI</b> %
~													
ALD 🗸	1		6.88 🕂 —	21.700(+-	9.80 + -	0.0000001 + -	AASHTO #3 (72)∽	1.00 + -	0.00 + -	19.80 +	84.0C + -	16.0C + —	0.00 + -
Conveyance Ditch 🗸	2		6.88 🕂 —	0.0500 + -	12.00 + -	0.0100000 + -	AASHTO #1 (45)∽	1.00 + -	0.00 + -	0.00 + -	100.C + -	0.00 + -	0.00 + -
Ponds 🗸	3	Water Layer	6.88 + -	20.000( +	12.00 +	0.0000100 + -	0 ~	1.00 + -	0.00 + -	10.00 + -	100.0 +	0.00 + -	0.00 + -
Conveyance Ditch 🗸	4	Water Layer	6.88 + -	0.0500 + -	12.00 +	0.0100000 + -	AASHTO #1 (45)∽	1.00 + -	0.00 + -	0.00 + -	100.0 + -	0.00 + -	0.00 + -
	5	Water Layer	6.88 + -	0.0000 + -	12.00 +	0.0000100 + -	0 ~	1.00 + -	0.00 + -	0.00 + -	100.0 +	0.00 + -	0.00 + -
Limestone Bed 🛛 🗸	6	Limestone Layer	6.88 + -	40.000( +	12.00 +	0.0000001 + -	AASHTO #1 (45)₩	1.00 + -	0.00 + -	20.00 + -	84.00 +	16.0C + —	0.00 + -
Conveyance Ditch 🗸	7	Water Layer	6.88 + -	0.0500 + -	12.00 +	0.0050000 + -	AASHTO #1 (45)∽	1.00 + -	0.00 + -	0.00 + -	100.0 +	0.00 + -	0.00 + -
Ponds 🗸	8	Water Layer	6.88 + -	8.0000 + -	12.00 +	0.0000100 + -	0 ~	1.00 + -	0.00 + -	0.00 + -	100.0 +	0.00 + -	0.00 + -
Conveyance Ditch 🗸	9	Water Layer	6.88 + -	0.0500 + -	12.00 +	0.0100000 + -	AASHTO #1 (45)₩	1.00 + -	0.00 + -	0.00 + -	100.0 + -	0.00 + -	0.00 + -
Mn Removal Bed 🗸	10	Limestone Layer	6.88 + -	5.0000 +	12.00 +	0.0000001 + -	\ASHTO #5 (144∨	1.00 + -	0.00 + -	50.00 + -	0.00 + -	100.0 + -	0.00 + -
Mn Removal Bed 🗸	11	Limestone Layer	6.88 + -	5.0000 +	12.00 +	0.0000001 + -	\ASHTO #5 (144∨	1.00 + -	0.00 + -	50.00 + -	0.00 + -	100.0 +	0.00 + -
	Total R	letention Time (hrs)	3	99.9									
•													
Model Outpu	ut												
	_												

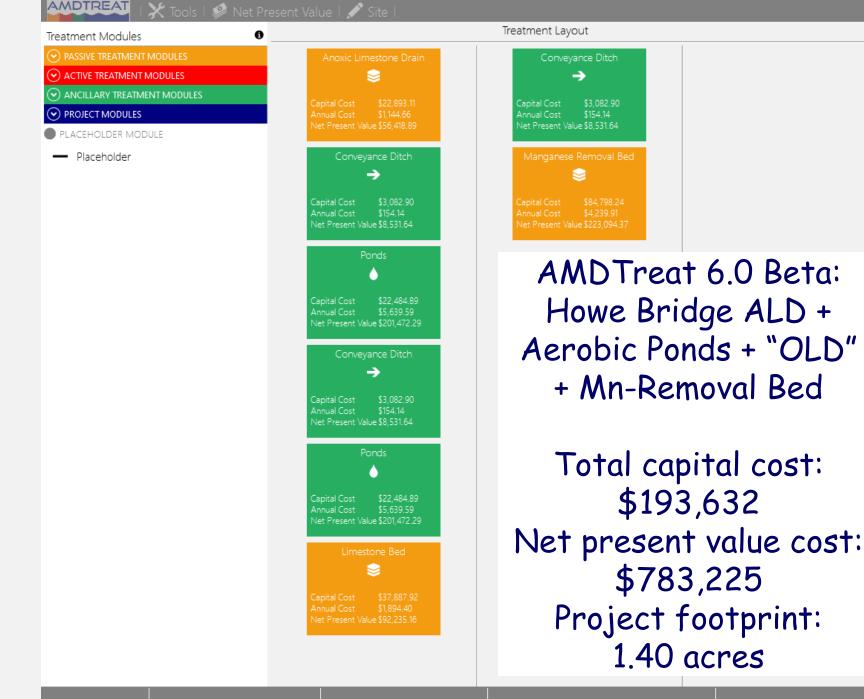
Print PHREEQC Output Report

Select Workspace C:\Users\cravotta\Documents\AMDTreat\_geochem\_data\AMDTreatBeta\HoweBrid

AMDTreat 6.0 Beta "PHREEQ-N-AMDTreat" tool (1) anoxic limestone drain; (3) aerobic pond; (5) oxic limestone bed; (7) aerobic pond; and (9-11) manganese removal bed with intermediate aeration steps (2, 4, 6, 8).

#### Howe Bridge ALD + Aerobic Ponds + OLD + Mn-Removal Bed





# Conclusions

- PHREEQ-N-AMDTreat tools that include equilibrium and kinetics models are useful to evaluate AMD treatment performance and design.
- Graphical and tabular output indicates the pH and solute concentrations in effluent plus quantity of precipitated solids.
- By adjusting kinetic variables or chemical dosing, various passive and/or active treatment strategies can be simulated.
- AMDTreat cost-analysis software can be used to evaluate the feasibility for installation and operation of treatments that produce the desired effluent quality.

# Disclaimer / Release Status

"Although this software program has been used by the U.S. Geological Survey (USGS), no warranty, expressed or implied, is made by the USGS or the U.S. Government as to the accuracy and functioning of the program and related program material nor shall the fact of distribution constitute any such warranty, and no responsibility is assumed by the USGS in connection therewith."

- ✓ FY2017-2020 Development, beta testing and review.
- FY2021 USGS software release, available for download: <u>https://doi.org/10.5066/P9QEE3D5</u>
- FY2021 Documentation, open-access Applied Geochemistry article: <u>https://doi.org/10.1016/j.apgeochem.2020.104845</u>
- FY2022 Incorporation with AMDTreat 6.0 for release by OSMRE: <u>https://www.osmre.gov/programs/reclaiming-abandoned-mine-lands/amdtreat</u>

### References

AMDTreat 6.0 Beta (2022) https://www.osmre.gov/programs/reclaiming-abandoned-mine-lands/amdtreat

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